## Blactmer

## Hydraulic Data For Pump Applications

For Blackmer Positive Displacement Sliding Vane Pumps

## HYDRAULIC DATA

This HYDRAULIC DATA BULLETIN was compiled by Blackmer's Engineering Department as an aid to operators, engineers, maintenance supervisors, equipment distributors, sales engineers, and Blackmer customers for planning installations of positive displacement rotary pumps. The Pipe Friction Curves were reprinted from the ENGINEERING DATA BOOK, First Edition, copyrighted 1979 by the Hydraulic Institute.

Blackmer Sales Offices, Distributors, and Application Engineers are available for assistance and recommendations in planning specific applications. Although this bulletin is not for sale, additional copies are available to all Blackmer customers.


Planning for a satisfactory and economical pump installation involves the two basic items of (1) selecting the proper type, size and speed of pumping equipment and
(2) making a careful study of the suction and discharge conditions, including all details of the piping layout.
The proper selection of pumping equipment must consider all of the application conditions to include these important factors. For specific selection of Blackmer Positive Displacement Rotary Pumps, please refer to our individual Pump Characteristic Curves.


How much flow?


How much push?


1. Approximate DELIVERY required in gallons per minute (G.P.M.).

## 2.

Differential
PRESSURE required in pounds per square inch (psi).
3.

Specific GRAVITY of the liquid.
4.

Maximum VISCOSITY of the liquid in Seconds Saybolt Universal (SSU).


How hot?


How much pull?


What liquid?

How long?

## 5.

Pumping
TEMPERATURE of the liquid in degrees Fahrenheit.
6.

SUCTION
conditions when pumping in inches of mercury for vacuum, or psi for pressure.

## 7.

Type of LIQUID to be handled.
8.

Type of SERVICE, i.e. intermittent duty, semi-continuous duty, or continuous duty.

## DEFINITIONS of HYDRAULIC TERMS

The Hydraulic Institute has made a study of hydraulic terms in an effort to establish standardization of definitions. Their recommendations are as follows:

Head - is the hydraulic pressure and is expressed in pounds-per-square-inch (psi) gauge using atmospheric pressure as the datum. It can be determined by use of pressure gauges or can be computed by using pipe friction tables and static head measurements.

Frictional Head - is the hydraulic pressure exerted to overcome frictional resistance of a piping system to the liquid flowing through it.

Static Suction Lift - is the hydraulic pressure be low atmospheric at the intake port with the liquid at rest. It is usually expressed in or converted to inches of mercury $(\mathrm{Hg})$ vacuum.

Total Suction Lift - is the total hydraulic pressure below atmospheric at the intake port with the pump in operation (the sum of the static suction lift and the friction head of the suction piping).

Flooded Suction - is a very indefinite term which has been carelessly used for so many years that its meaning is no longer clear. More often than not, it merely indicates that suction conditions have not been accurately determined. One point to remember is that a static suction head may become a suction lift when the pump goes into operation.

Total Suction Head - is the hydraulic pressure above atmospheric at the intake port with the pump in operation (the difference between the static suction head and the friction head of the suction piping).

Static Discharge Head - is the hydraulic pressure exerted at the pump discharge by the liquid at rest, commonly measured as the difference in elevation between the pump discharge port and the delivery port.

Total Discharge Head - is the total hydraulic pressure at the discharge port with the pump in operation (the sum of the static discharge head and the friction head of the discharge piping).

Total Pumping Head (or Dynamic Head) - is the sum of the total discharge head and the total suction lift; or the difference between the total discharge head and the total suction head.

Head Expressed in Feet - although the foregoing definitions refer to the "head" as expressed in psi, it is also proper to specify the total pumping head in feet of liquid or feet of water. Conversions can be made between these expressions of psi to feet (See chart on Page 6), but since there will normally be an appreciable difference between the feet of head of a particular liquid and the feet of head of water, it is extremely important to specify which term is being used.

## COMPUTING SUCTION \& DISCHARGE CONDITIONS

Two methods are outlined in this bulletin for computing suction and discharge conditions: (1) by using the direct-reading charts for quick preliminary computations, and (2) by using the Intake and Discharge Analysis Form (Page 12) in conjunction with the Hydraulic Institute friction loss curves (Pages 13 thru 19).

## FIRST PROCEDURE (using the direct-reading charts)

## Total Suction Lift

(1) Given the maximum static lift in feet, determine the static vacuum in inches of mercury $(\mathrm{Hg})$ from chart at top of Page 5.
(2) Compute total equivalent length of pipe in suction line by using the chart on Page 11.
(3) Read friction loss in inches of mercury per 100 ft . of pipe from the direct reading charts (Pages 7 thru 10). Multiply this value by the total equivalent length of pipe and divide by 100.
(4) Add this friction loss to the static suction lift to obtain the total suction lift.

## Total Discharge Head

(1) Follow the same procedure as in steps 1 and 2 above but refer to static discharge head chart on Page 6.
(2) Refer to the direct-reading charts as in step 3 above, but read friction loss from the psi column.
(3) Add this friction loss to the static discharge head to obtain the total discharge head.

## example

## DATA

Liquid to be pumped .............gasoline
Gallons per minute ............... 90
Static suction lift. ..................10' liquid
Suction line .......................... $43^{\prime}$ of $21 / 2$ pipe, with one $2 \frac{1}{2} /{ }^{\prime \prime}$ elbow
Static discharge head ...........40' liquid
Discharge line......................80' of 2" pipe, with 5 elbows

## SUCTION

1. From static lift chart (p. 5), 10 ' lift=6.4 in. $\mathrm{Hg} \quad 6.4 \mathrm{in} . \mathrm{Hg}$
2. Total equivalent length suction pipe (from page 11) $=43^{\prime}+7^{\prime}=50 "$
3. From Table (Page 8), friction per $100 \mathrm{O}=3.7 \mathrm{in} . \mathrm{Hg}$
4. Frictional head of suction piping $\frac{50 \times 3.7}{100}=1.9 \mathrm{in} . \mathrm{Hg} 1.9 \mathrm{in} . \mathrm{Hg}$ Total suction lift $\quad 8.3 \mathrm{in}$. Hg

## DISCHARGE

1. From static head chart (Page 6), $40^{\prime}$ head $=12.5 \mathrm{psi} 12.5 \mathrm{psi}$
2. Total equivalent length discharge pipe (from page 11) $=80+(5 \times 5)=105^{\prime}$
3. From table (Page 8), friction per $100 \mathrm{O}=4.4 \mathrm{psi}$
4. Frictional head of discharge piping $\frac{105 \times 4.4}{100}=4.6 \mathrm{psi} \quad 4.6 \mathrm{psi}$
5. Total discharge head
17.1 psi

NOTE: To determine the required horsepower, first convert the total suction lift from in. Hg to psi (using the pressure conversion factors on page 21). Then add this value to the total discharge head to obtain the total pumping or dynamic head, from which the required horsepower can be determined using Blackmer Characteristic Curves printed separately.

## TYPICAL ROTARY PUMP INSTALLATION

Rotary pumps are used extensively for difficult liquid applications involving volatile or viscous liquids. Consequently it is of utmost importance that a careful study be made of each application to be certain that proper size suction and discharge piping will be used and that the pump be located most advantageously in relation to the liquid source. Remember that it is always easier to push a liquid than to pull it.


STATIC SUCTION LIFT

Although the suction condition is commonly the last factor considered in planning a pump installation, experience proves that for a majority of applications this will be the most important factor. It is always desirable to plan the installation so that a minimum suction lift is required, particularly when handling volatile liquids (or even some viscous liquids which include "light ends" that may be vaporized under vacuum); or liquids which are so viscous that it is difficult to pull them through a suction pipe. Remember that if a pump is "starved" for liquid, the result will be excessive cavitation, vibration, and a noticeable reduction in the delivery rate.

## STATIC LIFT CONVERSION CHART



FRICTION LOSS in SMOOTH-BORE RUBBER HOSE

| U.S. Gal. Per Min. | ACTUAL INSIDE DIAMETER IN INCHES |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 3/4 | 1 | 11/4 | 11/2 | 2 | 21/2 | 3 | 4 |
| 15 | 30.0 | 8.9 | 2.5 | 1.1 | 0.4 | 0.1 |  |  |
| 20 | 53.0 | 14.0 | 4.3 | 1.8 | 0.7 | 0.2 |  |  |
| 25 | 79.0 | 22.0 | 6.5 | 2.9 | 1.0 | 0.3 |  |  |
| 30 | 112.0 | 31.0 | 9.2 | 4.0 | 1.4 | 0.4 | 0.1 |  |
| 40 |  | 53.0 | 15.0 | 6.7 | 2.4 | 0.6 | 0.3 |  |
| 50 |  | 80.0 | 24.0 | 10.0 | 3.6 | 1.0 | 0.5 |  |
| 60 |  | 101.0 | 35.0 | 14.0 | 5.1 | 1.4 | 0.6 |  |
| 70 |  |  | 45.0 | 19.0 | 6.6 | 1.8 | 0.8 |  |
| 80 |  |  | 58.0 | 24.0 | 8.6 | 2.3 | 1.1 |  |
| 90 |  |  | 71.0 | 30.0 | 11.0 | 3.0 | 1.4 | 0.3 |
| 100 |  |  | 88.0 | 37.0 | 12.5 | 3.5 | 1.7 | 0.4 |
| 125 |  |  | 132.0 | 55.0 | 20.0 | 5.3 | 2.5 | 0.6 |
| 150 |  |  | 183.0 | 78.0 | 27.0 | 7.5 | 3.5 | 0.7 |
| 175 |  |  |  | 100.0 | 37.0 | 10.0 | 4.6 | 1.1 |
| 200 |  |  |  | 133.0 | 46.0 | 13.0 | 5.9 | 1.4 |
| 250 |  |  |  |  | 70.0 | 19.0 | 9.1 | 2.1 |
| 300 |  |  |  |  | 95.0 | 27.0 | 12.0 | 2.9 |
| 350 |  |  |  |  | 126.0 | 36.0 | 17.0 | 4.0 |
| 400 |  |  |  |  |  | 46.0 | 21.0 | 5.1 |
| 500 |  |  |  |  |  | 70.0 | 32.0 | 7.4 |
| 600 |  |  |  |  |  | 105.0 | 46.0 | 10.0 |
| 700 |  |  |  |  |  | 148.0 | 62.0 | 13.0 |
| 800 |  |  |  |  |  | 190.0 | 79.0 | 17.0 |
| 900 |  |  |  |  |  |  | 97.0 | 22.0 |
| 1000 |  |  |  |  |  |  | 116.0 | 27.0 |
| 1250 |  |  |  |  |  |  | 170.0 | 43.0 |
| 1500 |  |  |  |  |  |  | 226.0 | 61.0 |
| 1750 |  |  |  |  |  |  |  | 80.0 |
| 2000 |  |  |  |  |  |  |  | 100.0 |

Note: Data shown is for liquid having specific gravity of 1 and a viscosity of 30 SSU.

## STATIC HEAD CONVERSION CHART



## DIRECT-READING FRICTION TABLES

HOW TO USE THE FRICTION TABLES: These tables, based on data from the Standards of the Hydraulic Institute, show the friction loss (in PSI or inches of Mercury) for 100 feet of pipe. Values in the white area are proportional to GPM and viscosity and may be interpolated. Values in the shaded area are for new pipe only. (Multiply by 1.4 to calculate losses for 15 -year-old pipe.) IMPORTANT: Note that sample liquids at the top of each column have different specific gravities. In all cases, be sure to divide the friction loss by the specific gravity of
the sample liquid and multiply it by the specific gravity of the liquid being transferred. For example, the friction loss per hundred feet of 2-inch pipe when pumping a liquid of 2000 SSU at 100 GPM would be half way between 28.8 PSI (the loss for 1000 SSU ) and 86.4 PSI (the loss for 3000 SSU) or in other words 57.6 PSI ... if the liquid had a specific gravity of .9. However, if the liquid had a specific gravity of say 1.1, then the friction loss per hundred feet would be 57.6 divided by .9 and multiplied by 1.1 , or 70.4 PSI.

| PIPE <br> SIZE | GPM | GASOLINE SP. GR. . 72 |  | WATER SP. GR. 1 |  | NO. 2 FUEL OIL SP. GR. 84 50 SSU |  | $\begin{gathered} \text { OIL } \\ \text { SP. GR. . } 9 \\ 500 \text { SSU } \end{gathered}$ |  | $\begin{aligned} & \text { OIL } \\ & \text { SP. GR. . } 9 \\ & 1000 \text { SSU } \end{aligned}$ |  | $\begin{gathered} \text { OIL } \\ \text { SP. GR. . } 9 \\ 3000 \text { SSU } \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | PSI | IN. HG. | PSI | IN. HG. | PSI | IN. HG. | PSI | IN. HG. | PSI | IN. HG. | PSI | IN. HG. |
| 1/2" | 2 | 1.3 | 2.7 | 2.1 | 4.3 | 2.3 | 4.7 | 35.5 | 73 | 71 | 145 | 213 | 435 |
|  | 4 | 4.8 | 9.8 | 7.6 | 15.5 | 8.8 | 18.0 | 71.0 | 145 | 145 | 296 | 435 | 888 |
|  | 6 | 10.8 | 22.1 | 16.5 | 33.7 | 18.5 | 37.8 | 107.0 | 219 | 216 | 442 | 648 | 1326 |
|  | 8 | 18.5 | 37.8 | 28.0 | 57.2 | 31.0 | 63.5 | 145.0 | 296 | 280 | 572 | 840 | 1716 |
|  | 10 | 28.8 | 58.9 | 42.0 | 85.8 | 46.0 | 94.0 | 175.0 | 358 | 355 | 725 | 1065 | 2175 |
| 3/4" | 5 | 1.8 | 3.7 | 2.8 | 5.7 | 3.4 | 7.0 | 29 | 59 | 57 | 117 | 170 | 348 |
|  | 10 | 6.7 | 13.7 | 10.2 | 20.9 | 11.5 | 23.5 | 57 | 117 | 117 | 239 | 351 | 718 |
|  | 15 | 15.2 | 31.1 | 22.0 | 45.0 | 25.0 | 51.1 | 87 | 178 | 170 | 348 | 510 | 1042 |
|  | 20 | 26.0 | 53.1 | 39.0 | 80.0 | 42.0 | 86.0 | 117 | 239 | 230 | 470 | 690 | 1410 |
| 1" | 5 | 0.6 | 1.2 | 0.8 | 1.6 | 1.0 | 2.0 | 10.8 | 22.0 | 21.6 | 44.0 | 64.8 | 132.3 |
|  | 10 | 2.1 | 4.3 | 2.7 | 5.5 | 3.6 | 7.3 | 21.6 | 44.0 | 43.2 | 88.2 | 129.6 | 264.6 |
|  | 15 | 4.4 | 9.0 | 6.5 | 13.3 | 7.6 | 15.5 | 32.4 | 66.1 | 64.8 | 132.3 | 194.4 | 396.9 |
|  | 20 | 7.9 | 16.1 | 11.5 | 23.5 | 12.6 | 27.7 | 43.2 | 88.2 | 86.4 | 176.4 | 259.2 | 529.2 |
|  | 25 | 11.9 | 24.3 | 17.3 | 35.3 | 18.9 | 38.6 | 54.0 | 110.2 | 108.0 | 220.5 | 324.0 | 661.5 |
|  | 30 | 17.6 | 35.9 | 25.0 | 51.0 | 26.9 | 54.9 | 64.8 | 132.3 | 129.6 | 264.6 | 388.8 | 793.8 |
|  | 35 | 23.0 | 47.0 | 33.0 | 67.4 | 35.3 | 72.1 | 75.6 | 154.3 | 151.2 | 308.7 | 453.6 | 926.1 |
|  | 40 | 30.6 | 62.5 | 43.0 | 87.8 | 44.5 | 90.9 | 86.4 | 176.4 | 172.8 | 352.8 | 518.4 | 1058.4 |
| 11/4" | 5 | 0.1 | 0.4 | 0.2 | 0.4 | 0.3 | 0.6 | 3.6 | 7.3 | 7.2 | 14.7 | 21.6 | 44.1 |
|  | 10 | 0.5 | 1.0 | 0.8 | 1.6 | 1.0 | 2.0 | 7.2 | 14.7 | 14.4 | 29.4 | 43.2 | 88.2 |
|  | 15 | 1.2 | 2.4 | 1.7 | 3.5 | 2.0 | 4.1 | 10.8 | 22.0 | 21.6 | 44.1 | 64.8 | 132.3 |
|  | 20 | 2.0 | 4.1 | 2.8 | 5.7 | 3.4 | 6.9 | 14.4 | 29.4 | 28.8 | 58.8 | 86.4 | 176.4 |
|  | 25 | 3.0 | 6.1 | 4.3 | 8.8 | 5.0 | 10.2 | 18.0 | 36.7 | 36.0 | 73.5 | 108.0 | 220.5 |
|  | 30 | 4.2 | 8.6 | 6.0 | 12.2 | 7.1 | 14.5 | 21.6 | 44.1 | 43.2 | 88.2 | 129.6 | 264.6 |
|  | 35 | 5.8 | 11.8 | 8.2 | 16.7 | 9.5 | 19.4 | 25.2 | 51.4 | 50.4 | 102.9 | 151.2 | 308.7 |
|  | 40 | 7.6 | 15.5 | 11.0 | 22.4 | 11.8 | 24.1 | 28.8 | 58.8 | 57.6 | 117.6 | 172.8 | 352.8 |
|  | 45 | 9.4 | 19.2 | 13.5 | 27.6 | 14.7 | 30.0 | 32.4 | 66.1 | 64.8 | 132.3 | 196.4 | 401.0 |
|  | 50 | 11.5 | 23.5 | 16.3 | 33.2 | 17.6 | 35.9 | 36.0 | 73.5 | 72.0 | 147.0 | 216.0 | 441.0 |
|  | 60 | 16.6 | 33.9 | 23.0 | 47 | 24.4 | 50 | 45.0 | 91.9 | 90.0 | 183.7 | 270.0 | 551.2 |
|  | 70 | 22.3 | 45.6 | 31.0 | 63 | 32.0 | 65 | 54 | 111 | 101 | 207 | 303 | 620 |
|  | 80 | 28.8 | 59 | 40.0 | 82 | 40 | 82 | 72 | 147 | 115 | 235 | 345 | 705 |
|  | 90 | 36.0 | 74 | 50.0 | 102 | 50 | 102 | 89 | 182 | 129 | 264 | 387 | 790 |
| 11/2" | 5 | 0.1 | 0.2 | 0.1 | 0.2 | 0.1 | 0.2 | 2.0 | 4.1 | 4.5 | 8.2 | 12.0 | 24.5 |
|  | 10 | 0.2 | 0.6 | 0.4 | 0.8 | 0.5 | 1.0 | 4.0 | 8.2 | 8.0 | 16.3 | 24.0 | 49.0 |
|  | 15 | 0.5 | 1.0 | 0.8 | 1.6 | 0.9 | 1.8 | 5.9 | 12.2 | 12.0 | 24.0 | 36.0 | 73.5 |
|  | 20 | 0.9 | 1.8 | 1.3 | 2.7 | 1.6 | 3.3 | 8.1 | 16.3 | 16.0 | 32.6 | 48.0 | 98.0 |
|  | 25 | 1.4 | 2.9 | 2.0 | 4.2 | 2.3 | 4.7 | 10.0 | 20.4 | 20.0 | 40.8 | 60.0 | 122.5 |
|  | 30 | 2.0 | 3.9 | 2.9 | 5.9 | 3.3 | 6.9 | 12.0 | 24.5 | 24.0 | 49.0 | 72.0 | 147.0 |
|  | 35 | 2.6 | 5.2 | 3.7 | 7.5 | 4.2 | 8.6 | 14.0 | 28.6 | 28.0 | 57.2 | 84.0 | 171.5 |
|  | 40 | 3.3 | 6.7 | 4.8 | 9.8 | 5.5 | 11.2 | 16.0 | 32.6 | 32.0 | 65.3 | 96.0 | 196.0 |
|  | 45 | 4.2 | 8.6 | 6.0 | 12.2 | 6.7 | 13.7 | 18.0 | 36.8 | 36.0 | 73.5 | 108.0 | 225.5 |
|  | 50 | 5.1 | 10.4 | 7.4 | 15.1 | 8.4 | 17.1 | 20.0 | 40.8 | 40.0 | 81.7 | 120.0 | 245.0 |
|  | 60 | 7.6 | 15.5 | 11.0 | 22.4 | 11.8 | 24.0 | 24.0 | 49.0 | 48.0 | 98.0 | 144.0 | 294.0 |
|  | 70 | 10.1 | 20.6 | 14.6 | 29.8 | 15.6 | 31.8 | 28.0 | 57.1 | 56.0 | 114.3 | 168.0 | 343.0 |
|  | 80 | 13.0 | 26.6 | 18.5 | 37.8 | 20.1 | 41.0 | 32.0 | 65.3 | 64.0 | 130.7 | 192.0 | 392.0 |
|  | 100 | 19.5 | 40 | 28.0 | 57 | 29 | 59 | 51 | 104 | 80 | 164 | 240 | 491 |
|  | 120 | 28 | 57 | 41 | 84 | 42 | 86 | 73 | 149 | 96 | 196 | 288 | 589 |

HOW TO USE THE FRICTION TABLES: These tables, based on data from the Standards of the Hydraulic Institute, show the friction loss (in PSI or inches of Mercury) for 100 feet of pipe. Values in the white area are proportional to GPM and viscosity and may be interpolated. Values in the shaded area are for new pipe only. (Multiply by 1.4 to calculate losses for 15 -year-old pipe.) IMPORTANT: Note that sample liquids at the top of each column have different specific gravities. In all cases, be sure to divide the friction loss by the specific gravity of
the sample liquid and multiply it by the specific gravity of the liquid being transferred. For example, the friction loss per hundred feet of 2-inch pipe when pumping a liquid of 2000 SSU at 100 GPM would be half way between 28.8 PSI (the loss for 1000 SSU ) and 86.4 PSI (the loss for 3000 SSU) or in other words 57.6 PSI ... if the liquid had a specific gravity of .9. However, if the liquid had a specific gravity of say 1.1, then the friction loss per hundred feet would be 57.6 divided by .9 and multiplied by 1.1, or 70.4 PSI.

| PIPE SIZE | GPM | GASOLINE SP. GR. . 72 |  | WATER SP. GR. 1 |  | $\begin{aligned} & \text { NO. } 2 \text { FUEL OIL } \\ & \text { SP. GR. } 84 \\ & 50 \text { SSU } \end{aligned}$ |  | $\begin{gathered} \text { OIL } \\ \text { SP. GR. . } 9 \\ 500 \text { SSU } \end{gathered}$ |  | $\begin{aligned} & \text { OIL } \\ & \text { SP. GR. . } 9 \\ & 1000 \text { SSU } \end{aligned}$ |  | $\begin{aligned} & \text { OIL } \\ & \text { SP. GR. . } 9 \\ & 3000 \text { SSU } \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | PSI | IN. HG. | PSI | IN. HG. | PSI | IN. HG. | PSI | IN. HG. | PSI | IN. HG. | PSI | IN. HG. |
| 2" | 10 | 0.1 | 0.2 | 0.1 | 0.2 | 0.1 | 0.2 | 1.4 | 2.9 | 2.8 | 5.7 | 8.4 | 17.1 |
|  | 15 | 0.1 | 0.2 | 0.2 | 0.4 | 0.3 | 0.6 | 2.1 | 4.3 | 4.2 | 8.6 | 12.6 | 25.7 |
|  | 20 | 0.2 | 0.4 | 0.4 | 0.8 | 0.4 | 0.8 | 2.8 | 5.7 | 5.6 | 11.4 | 16.8 | 34.2 |
|  | 25 | 0.4 | 0.8 | 0.6 | 1.2 | 0.7 | 1.4 | 3.6 | 7.3 | 7.2 | 14.7 | 21.6 | 44.0 |
|  | 30 | 0.5 | 1.0 | 0.8 | 1.6 | 0.9 | 1.8 | 4.2 | 8.6 | 8.4 | 17.1 | 25.2 | 51.5 |
|  | 35 | 0.7 | 1.4 | 1.1 | 2.2 | 1.3 | 2.7 | 4.9 | 10.0 | 9.8 | 20.0 | 29.4 | 60.0 |
|  | 40 | 0.9 | 1.8 | 1.3 | 2.7 | 1.5 | 3.1 | 5.6 | 11.4 | 11.2 | 22.8 | 33.6 | 68.6 |
|  | 45 | 1.2 | 2.4 | 1.7 | 3.5 | 1.9 | 3.9 | 6.3 | 12.9 | 12.6 | 25.7 | 37.8 | 77.2 |
|  | 50 | 1.4 | 2.9 | 2.1 | 4.3 | 2.4 | 4.9 | 7.2 | 14.7 | 14.4 | 29.4 | 43.2 | 88.2 |
|  | 60 | 2.0 | 4.1 | 3.0 | 6.1 | 3.4 | 6.9 | 8.6 | 17.5 | 17.2 | 35.1 | 51.6 | 105.3 |
|  | 70 | 2.7 | 5.5 | 4.0 | 8.2 | 4,4 | 9.0 | 10.1 | 20.6 | 20.2 | 41.2 | 60.6 | 123.7 |
|  | 80 | 3.4 | 6.9 | 5.0 | 10.2 | 5.6 | 11.4 | 11.5 | 23.5 | 23.0 | 47.0 | 69.0 | 140.9 |
|  | 90 | 4.4 | 9.0 | 6.2 | 12.7 | 6.9 | 14.1 | 12.9 | 26.4 | 25.8 | 52.7 | 77.4 | 158.0 |
|  | 100 | 5.4 | 11.0 | 7.8 | 16.3 | 8.4 | 17.1 | 14.4 | 29.4 | 28.8 | 58.8 | 86.4 | 176.4 |
|  | 120 | 7.9 | 15.1 | 11.6 | 23.7 | 12.1 | 20.7 | 20.7 | 41.2 | 34.4 | 70.2 | 103.2 | 210.7 |
|  | 140 | 10.1 | 20.6 | 15.0 | 30.7 | 15.5 | 31.7 | 28 | 57 | 40 | 82 | 120 | 245 |
|  | 160 | 13.0 | 26.6 | 19.0 | 38.8 | 20.0 | 40.8 | 36 | 74 | 45 | 92 | 135 | 276 |
|  | 180 | 17.0 | 34.8 | 23.5 | 48.0 | 25.0 | 51.1 | 46 | 94 | 51 | 104 | 153 | 313 |
|  | 200 | 20.5 | 42.0 | 28.5 | 58.3 | 30.0 | 61.4 | 58 | 118 | 56 | 115 | 168 | 343 |
| 21/2" | 20 | 0.1 | 0.2 | 0.2 | 0.4 | 0.2 | 0.4 | 1.4 | 2.9 | 2.8 | 5.7 | 8.4 | 17.1 |
|  | 25 | 0.2 | 0.4 | 0.2 | 0.4 | 0.3 | 0.6 | 1.8 | 3.7 | 3.6 | 7.3 | 10.8 | 22.0 |
|  | 30 | 0.2 | 0.4 | 0.3 | 0.6 | 0.4 | 0.8 | 2.2 | 4.5 | 4.4 | 9.0 | 13.2 | 26.9 |
|  | 35 | 0.3 | 0.6 | 0.4 | 0.8 | 0.5 | 1.0 | 2.5 | 5.1 | 5.0 | 10.2 | 15.0 | 30.6 |
|  | 40 | 0.4 | 0.8 | 0.6 | 1.2 | 0.7 | 1.4 | 2.9 | 5.9 | 5.8 | 11.8 | 17.4 | 35.0 |
|  | 45 | 0.5 | 1.0 | 0.7 | 1.4 | 0.8 | 1.6 | 3.2 | 6.5 | 6.4 | 13.1 | 19.2 | 39.2 |
|  | 50 | 0.6 | 1.2 | 0.9 | 1.8 | 1.0 | 2.0 | 3.6 | 7.3 | 7.2 | 14.7 | 21.6 | 44.0 |
|  | 60 | 0.9 | 1.8 | 1.2 | 2.4 | 1.4 | 2.9 | 4.3 | 8.8 | 8.6 | 17.5 | 25.8 | 52.5 |
|  | 70 | 1.2 | 2.4 | 1.6 | 3.3 | 1.9 | 3.9 | 5.0 | 10.2 | 10.0 | 20.4 | 30.0 | 61.2 |
|  | 80 | 1.4 | 2.9 | 2.0 | 4.1 | 2.4 | 4.9 | 5.8 | 11.8 | 11.6 | 23.6 | 34.8 | 71.0 |
|  | 90 | 1.8 | 3.7 | 2.5 | 5.1 | 2.9 | 5.9 | 6.5 | 13.3 | 13.0 | 26.5 | 39.0 | 79.6 |
|  | 100 | 2.2 | 4.5 | 3.0 | 6.1 | 3.6 | 7.3 | 7.2 | 14.7 | 14.4 | 29.4 | 43.2 | 88.2 |
|  | 120 | 3.1 | 6.3 | 4.5 | 9.2 | 5.0 | 10.2 | 8.6 | 17.5 | 17.2 | 35.1 | 57.6 | 117.6 |
|  | 140 | 4.1 | 8.4 | 6.0 | 12.2 | 6.6 | 13.5 | 11.3 | 23.0 | 20.2 | 41.2 | 60.6 | 123.7 |
|  | 160 | 5.4 | 11.0 | 7.8 | 15.9 | 8.4 | 17.1 | 15.1 | 30.8 | 23.0 | 47.0 | 69.0 | 140.9 |
|  | 180 | 6.9 | 14.1 | 10.0 | 20.4 | 10.5 | 21.4 | 19.8 | 40.5 | 25.9 | 52.9 | 77.7 | 158.6 |
|  | 200 | 8.6 | 17.5 | 12.0 | 24.5 | 12.6 | 25.7 | 23.9 | 48.8 | 28.8 | 58.8 | 86.4 | 176.4 |
|  | 220 | 9.5 | 19.5 | 13.8 | 28.2 | 14.3 | 29.2 | 26.5 | 54 | 31 | 64 | 93 | 190 |
|  | 240 | 11.9 | 24.3 | 16.5 | 33.7 | 17.5 | 35.8 | 32.5 | 66 | 34 | 70 | 103 | 211 |
|  | 260 | 13.7 | 28.0 | 19.3 | 39.4 | 20.5 | 42.0 | 37.0 | 75.5 | 38 | 78 | 113 | 231 |
| 3" | 30 | 0.1 | 0.2 | 0.1 | 0.2 | 0.1 | 0.2 | 0.9 | 1.8 | 1.8 | 3.7 | 5.4 | 11.0 |
|  | 35 | 0.1 | 0.2 | 0.1 | 0.2 | 0.2 | 0.4 | 1.1 | 2.2 | 2.1 | 4.3 | 6.3 | 12.9 |
|  | 40 | 0.1 | 0.2 | 0.2 | 0.4 | 0.2 | 0.4 | 1.2 | 2.4 | 2.4 | 4.9 | 7.2 | 14.7 |
|  | 45 | 0.2 | 0.4 | 0.2 | 0.4 | 0.3 | 0.6 | 1.3 | 2.7 | 2.7 | 5.5 | 8.1 | 16.5 |
|  | 50 | 0.2 | 0.4 | 0.3 | 0.6 | 0.3 | 0.6 | 1.5 | 3.1 | 3.0 | 6.1 | 9.0 | 18.3 |
|  | 60 | 0.3 | 0.6 | 0.4 | 0.8 | 0.5 | 1.0 | 1.8 | 3.7 | 3.6 | 7.3 | 10.8 | 22.0 |
|  | 70 | 0.4 | 0.8 | 0.6 | 1.2 | 0.6 | 1.2 | 2.1 | 4.3 | 4.2 | 8.6 | 12.6 | 25.7 |
|  | 80 | 0.5 | 1.0 | 0.7 | 1.4 | 0.8 | 1.6 | 2.4 | 4.9 | 4.8 | 9.8 | 14.4 | 29.4 |
|  | 90 | 0.6 | 1.2 | 0.9 | 1.8 | 1.0 | 2.0 | 2.7 | 5.5 | 5.4 | 11.0 | 16.2 | 33.0 |
|  | 100 | 0.7 | 1.4 | 1.1 | 2.2 | 1.2 | 2.4 | 3.0 | 6.1 | 6.0 | 12.2 | 18.0 | $36.7$ |
|  | 120 | 1.0 | 2.0 | 1.5 | 3.1 | 1.7 | 3.5 | 3.6 | 7.3 | 7.2 | 14.7 | 21.6 | $44.0$ |

HOW TO USE THE FRICTION TABLES: These tables, based on data from the Standards of the Hydraulic Institute, show the friction loss (in PSI or inches of Mercury) for 100 feet of pipe. Values in the white area are proportional to GPM and viscosity and may be interpolated. Values in the shaded area are for new pipe only. (Multiply by 1.4 to calculate losses for 15-year-old pipe.) IMPORTANT: Note that sample liquids at the top of each column have different specific gravities. In all cases, be sure to divide the friction loss by the specific gravity of
the sample liquid and multiply it by the specific gravity of the liquid being transferred. For example, the friction loss per hundred feet of 2-inch pipe when pumping a liquid of 2000 SSU at 100 GPM would be half way between 28.8 PSI (the loss for 1000 SSU ) and 86.4 PSI (the loss for 3000 SSU) or in other words 57.6 PSI ... if the liquid had a specific gravity of .9. However, if the liquid had a specific gravity of say 1.1, then the friction loss per hundred feet would be 57.6 divided by .9 and multiplied by 1.1 , or 70.4 PSI.

| $\begin{aligned} & \text { PIPE } \\ & \text { SIZE } \end{aligned}$ | GPM | GASOLINE SP. GR. . 72 |  | WATER SP. GR. 1 |  | NO. 2 FUEL OIL SP. GR. . 84 50 SSU |  | $\begin{gathered} \text { OIL } \\ \text { SP. GR. . } 9 \\ 500 \text { SSU } \end{gathered}$ |  | OILSP. GR. . 91000 SSU |  | OIL SP. GR. . 9 3000 SSU |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | PSI | IN. HG. | PSI | IN. HG. | PSI | IN. HG. | PSI | IN. HG. | PSI | IN. HG. | PSI | IN. HG. |
| 3" | 140 | 1.4 | 2.9 | 2.0 | 4.1 | 2.2 | 4.5 | 4.2 | 8.6 | 8.4 | 17.1 | 25.2 | 51.4 |
|  | 160 | 1.8 | 3.7 | 2.6 | 5.3 | 2.9 | 5.9 | 5.0 | 10.2 | 9.6 | 19.6 | 28.8 | 58.8 |
|  | 180 | 2.3 | 4.7 | 3.3 | 6.7 | 3.6 | 7.3 | 6.3 | 12.9 | 10.8 | 22.0 | 32.4 | 66.1 |
|  | 200 | 2.7 | 5.5 | 4.0 | 8.2 | 4.2 | 8.6 | 8.1 | 16.5 | 12.0 | 24.4 | 36.0 | 73.5 |
|  | 250 | 4.2 | 8.6 | 6.0 | 12.2 | 6.4 | 13.1 | 12.2 | 24.7 | 15.0 | 30.6 | 45.0 | 91.9 |
|  | 300 | 6.1 | 12.4 | 8.7 | 17.7 | 9.2 | 18.8 | 18.0 | 36.7 | 18.0 | 36.7 | 54.0 | 110.2 |
|  | 350 | 7.9 | 16.2 | 11.5 | 23.5 | 11.8 | 24.1 | 24.3 | 50 | 24.3 | 50 | 62 | 127 |
|  | 400 | 10.2 | 20.9 | 15.0 | 30.7 | 15.3 | 31.3 | 28.4 | 58 | 31.5 | 64 | 71 | 145 |
|  | 450 | 12.9 | 26.4 | 18.7 | 38.2 | 19.0 | 38.9 | 35.5 | 73 | 40.5 | 83 | 80 | 164 |
| 4" | 60 | 0.1 | 0.2 | 0.1 | 0.2 | 0.1 | 0.2 | 0.6 | 1.2 | 1.2 | 2.5 | 3.6 | 7.3 |
|  | 70 | 0.1 | 0.2 | 0.1 | 0.2 | 0.2 | 0.4 | 0.7 | 1.4 | 1.4 | 2.9 | 4.2 | 8.6 |
|  | 80 | 0.1 | 0.2 | 0.2 | 0.4 | 0.2 | 0.4 | 0.8 | 1.6 | 1.6 | 3.3 | 4.8 | 9.8 |
|  | 90 | 0.2 | 0.4 | 0.2 | 0.4 | 0.3 | 0.6 | 0.9 | 1.8 | 1.8 | 3.7 | 5.4 | 11.0 |
|  | 100 | 0.2 | 0.4 | 0.3 | 0.6 | 0.3 | 0.6 | 1.0 | 2.0 | 2.0 | 4.1 | 6.0 | 12.2 |
|  | 120 | 0.3 | 0.6 | 0.4 | 0.8 | 0.5 | 1.0 | 1.2 | 2.4 | 2.4 | 4.9 | 7.2 | 14.7 |
|  | 140 | 0.3 | 0.6 | 0.5 | 1.0 | 0.6 | 1.2 | 1.4 | 2.9 | 2.8 | 5.7 | 8.4 | 17.1 |
|  | 160 | 0.4 | 0.8 | 0.7 | 1.4 | 0.8 | 1.6 | 1.6 | 3.3 | 3.2 | 6.5 | 9.6 | 19.6 |
|  | 180 | 0.6 | 1.2 | 0.8 | 1.6 | 1.0 | 2.0 | 1.8 | 3.7 | 3.6 | 7.3 | 10.8 | 22.0 |
|  | 200 | 0.7 | 1.4 | 1.0 | 2.0 | 1.2 | 2.4 | 2.0 | 4.1 | 4.0 | 8.2 | 12.0 | 24.5 |
|  | 250 | 1.0 | 2.0 | 1.5 | 3.1 | 1.8 | 3.7 | 3.2 | 6.5 | 5.0 | 10.2 | 13.0 | 30.6 |
|  | 300 | 1.5 | 3.1 | 2.2 | 4.5 | 2.4 | 4.9 | 4.5 | 9.2 | 6.0 | 12.2 | 18.0 | 36.7 |
|  | 350 | 2.0 | 4.1 | 2.9 | 5.9 | 3.2 | 6.5 | 6.3 | 12.9 | 7.1 | 14.3 | 21.0 | 42.8 |
|  | 400 | 2.6 | 5.3 | 3.7 | 7.5 | 4.0 | 8.2 | 8.1 | 16.5 | 8.1 | 16.5 | 24.3 | 49.0 |
|  | 450 | 3.3 | 6.7 | 4.6 | 9.4 | 5.0 | 10.2 | 10.1 | 20.6 | 10.1 | 20.6 | 27.0 | 55.0 |
|  | 500 | 4.0 | 8.2 | 5.8 | 11.8 | 6.1 | 12.4 | 12.4 | 25.3 | 12.4 | 25.3 | 30.2 | 61.2 |
|  | 550 | 4.8 | 9.8 | 6.8 | 13.9 | 7.4 | 15.1 | 14.8 | 30.3 | 15.3 | 31.3 | 33 | 67.5 |
|  | 600 | 5.7 | 11.7 | 8.1 | 16.6 | 8.7 | 17.8 | 16.3 | 32.3 | 18.0 | 36.8 | 36 | 73.6 |
|  | 650 | 6.8 | 13.9 | 9.4 | 19.2 | 9.9 | 20.2 | 20.0 | 41.0 | 22.0 | 45.0 | 39 | 79.8 |
| 6" | 100 | ---- | ---- | ---- | ---- | ---- | ---- | 0.2 | 0.4 | 0.4 | 0.8 | 1.2 | 2.4 |
|  | 120 | ---- | ---- | ---- | ---- | ---- | ---- | 0.2 | 0.4 | 0.5 | 1.0 | 1.4 | 2.9 |
|  | 140 | ---- | ---- | ---- | ---- | ---- | ---- | 0.3 | 0.6 | 0.6 | 1.2 | 1.7 | 3.5 |
|  | 160 | 0.1 | 0.2 | 0.1 | 0.2 | 0.1 | 0.2 | 0.3 | 0.6 | 0.6 | 1.2 | 1.9 | 3.9 |
|  | 180 | 0.1 | 0.2 | 0.1 | 0.2 | 0.1 | 0.2 | 0.4 | 0.8 | 0.7 | 1.4 | 2.1 | 4.3 |
|  | 200 | 0.1 | 0.2 | 0.1 | 0.2 | 0.2 | 0.4 | 0.4 | 0.8 | 0.8 | 1.6 | 2.4 | 4.9 |
|  | 250 | 0.1 | 0.2 | 0.2 | 0.4 | 0.2 | 0.4 | 0.5 | 1.0 | 1.0 | 2.0 | 3.0 | 6.1 |
|  | 300 | 0.2 | 0.4 | 0.3 | 0.6 | 0.3 | 0.6 | 0.6 | 1.2 | 1.2 | 2.4 | 3.6 | 7.3 |
|  | 350 | 0.3 | 0.6 | 0.4 | 0.8 | 0.4 | 0.8 | 0.8 | 1.6 | 1.4 | 2.9 | 4.2 | 8.6 |
|  | 400 | 0.3 | 0.6 | 0.5 | 1.0 | 0.6 | 1.2 | 1.1 | 2.2 | 1.6 | 3.3 | 4.8 | 9.8 |
|  | 450 | 0.4 | 0.8 | 0.6 | 1.2 | 0.7 | 1.4 | 1.4 | 2.9 | 1.8 | 3.7 | 5.4 | 11.0 |
|  | 500 | 0.5 | 1.0 | 0.7 | 1.4 | 0.8 | 1.6 | 1.7 | 3.5 | 2.0 | 4.1 | 6.0 | 12.2 |
|  | 600 | 0.7 | 1.4 | 1.1 | 2.2 | 1.2 | 2.4 | 2.4 | 4.9 | 2.4 | 4.9 | 7.2 | 14.7 |
|  | 700 | 1.0 | 2.0 | 1.4 | 2.9 | 1.6 | 3.3 | 3.4 | 6.9 | 3.4 | 6.9 | 8.4 | 17.1 |
|  | 800 | 1.3 | 2.7 | 1.8 | 3.7 | 1.9 | 3.9 | 4.2 | 8.6 | 4.2 | 8.6 | 9.6 | 19.6 |
|  | 900 | 1.6 | 3.3 | 2.3 | 4.7 | 2.4 | 4.9 | 5.4 | 11.0 | 5.4 | 11.0 | 10.8 | 22.0 |
|  | 1000 | 2.0 | 4.1 | 2.8 | 5.7 | 2.9 | 5.9 | 6.7 | 13.7 | 6.7 | 13.7 | 12.0 | 24.5 |
|  | 1200 | 2.8 | 5.7 | 4.0 | 8.2 | 4.2 | 8.6 | 10.0 | 20.2 | 9.9 | 20.2 | 14.4 | 29.4 |
|  | 1500 | 4.2 | 8.6 | 6.0 | 12.2 | 6.2 | 12.6 | 15.3 | 31.2 | 15.3 | 31.2 | 18.0 | 36.7 |
| 8" | 200 | ---- | ---- | ---- | ---- | ---- | ---- | 0.1 | 0.2 | 0.3 | 0.6 | 0.8 | 1.6 |
|  | 250 | -- | ---- | ---- | ---- | ---- | ---- | 0.2 | 0.4 | 0.3 | 0.6 | 1.0 | 2.0 |
|  | 300 | ---- | ---- | ---- | ---- | 0.1 | 0.2 | 0.2 | 0.4 | 0.4 | 0.8 | 1.2 | 2.4 |

## DIRECT-READING FRICTION TABLES

HOW TO USE THE FRICTION TABLES: These tables, based on data from the Standards of the Hydraulic Institute, show the friction loss (in PSI or inches of Mercury) for 100 feet of pipe. Values in the white area are proportional to GPM and viscosity and may be interpolated. Values in the shaded area are for new pipe only. (Multiply by 1.4 to calculate losses for 15-year-old pipe.) IMPORTANT: Note that sample liquids at the top of each column have different specific gravities. In all cases, be sure to divide the friction loss by the specific gravity of
the sample liquid and multiply it by the specific gravity of the liquid being transferred. For example, the friction loss per hundred feet of 2 -inch pipe when pumping a liquid of 2000 SSU at 100 GPM would be half way between 28.8 PSI (the loss for 1000 SSU ) and 86.4 PSI (the loss for 3000 SSU) or in other words 57.6 PSI ... if the liquid had a specific gravity of .9. However, if the liquid had a specific gravity of say 1.1, then the friction loss per hundred feet would be 57.6 divided by .9 and multiplied by 1.1, or 70.4 PSI.

| PIPE <br> SIZE | GPM | GASOLINE SP. GR. . 72 |  | WATER <br> SP. GR. 1 |  | $\begin{gathered} \text { NO. } 2 \text { FUEL OIL } \\ \text { SP. GR. . } 84 \\ 50 \text { SSU } \\ \hline \end{gathered}$ |  | OIL SP. GR. . 9 500 SSU |  | OIL SP. GR. . 9 1000 SSU |  | OIL SP. GR. . 9 3000 SSU |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | PSI | IN. HG. | PSI | IN. HG. | PSI | IN. HG. | PSI | IN. HG. | PSI | IN. HG. | PSI | IN. HG. |
| 8" | 350 | ---- | ---- | 0,1 | 0.2 | 0.1 | 0.2 | 0.2 | 0.4 | 0.5 | 1.0 | 1.4 | 2.9 |
|  | 400 | ---- | ---- | 0.1 | 0.2 | 0.1 | 0.2 | 0.3 | 0.6 | 0.5 | 1.0 | 1.6 | 3.3 |
|  | 450 | 0.1 | 0.2 | 0.2 | 0.4 | 0.2 | 0.4 | 0.3 | 0.6 | 0.6 | 1.2 | 1.8 | 3.7 |
|  | 500 | 0.1 | 0.2 | 0.2 | 0.4 | 0.2 | 0.4 | 0.4 | 0.8 | 0.7 | 1.4 | 2.0 | 4.1 |
|  | 600 | 0.2 | 0.4 | 0.3 | 0.6 | 0.3 | 0.6 | 0.6 | 1.2 | 0.8 | 1.6 | 2.4 | 4.9 |
|  | 700 | 0.2 | 0.4 | 0.4 | 0.8 | 0.4 | 0.8 | 0.8 | 1.6 | 1.0 | 2.0 | 2.8 | 5.7 |
|  | 800 | 0.3 | 0.6 | 0.5 | 1.0 | 0.5 | 1.0 | 1.1 | 2.2 | 1.1 | 2.2 | 3.2 | 6.5 |
|  | 900 | 0.4 | 0.8 | 0.6 | 1.2 | 0.6 | 1.2 | 1.4 | 2.9 | 1.4 | 2.9 | 3.6 | 7.3 |
|  | 1000 | 0.5 | 1.0 | 0.7 | 1.4 | 0.8 | 1.6 | 1.5 | 3.5 | 1.7 | 3.5 | 4.0 | 8.2 |
|  | 1200 | 0.7 | 1.4 | 1.0 | 2.0 | 1.1 | 2.2 | 2.3 | 4.7 | 2.3 | 4.7 | 4.8 | 9.8 |
|  | 1500 | 1.0 | 2.0 | 1.5 | 3.1 | 1.6 | 3.3 | 3.8 | 7.8 | 3.8 | 7.8 | 6.0 | 12.2 |
|  | 1800 | 1.5 | 3.1 | 2.1 | 4.3 | 2.3 | 4.7 | 4.4 | 9.0 | 5.3 | 10.8 | 7.2 | 14.7 |
|  | 2100 | 2.0 | 4.1 | 2.8 | 5.7 | 3.0 | 6.1 | 6.0 | 12.3 | 7.2 | 14.7 | 8.3 | 17.0 |
| 10" | 450 | -- | -- | ---- | ---- | --- | ---- | 0.1 | 0.2 | 0.2 | 0.4 | 0.7 | 1.4 |
|  | 500 | -- | - | -- | -- | 0.1 | 0.2 | 0.1 | 0.2 | 0.3 | 0.6 | 0.8 | 1.6 |
|  | 600 | -- | - | -- | -- | 0.1 | 0.2 | 0.2 | 0.4 | 0.3 | 0.6 | 1.0 | 2.0 |
|  | 700 | 0.1 | 0.2 | 0.1 | 0.2 | 0.1 | 0.4 | 0.3 | 0.6 | 0.4 | 0.8 | 1.1 | 2.2 |
|  | 800 | 0.1 | 0.2 | 0.2 | 0.4 | 0.2 | 0.4 | 0.4 | 0.8 | 0.4 | 0.8 | 1.3 | 2.7 |
|  | 900 | 0.1 | 0.2 | 0.2 | 0.4 | 0.2 | 0.4 | 0.4 | 0.8 | 0.5 | 1.0 | 1.4 | 2.9 |
|  | 1000 | 0.1 | 0.2 | 0.2 | 0.4 | 0.3 | 0.6 | 0.5 | 1.0 | 0.5 | 1.0 | 1.6 | 3.3 |
|  | 1200 | 0.2 | 0.4 | 0.3 | 0.6 | 0.4 | 0.8 | 0.8 | 1.4 | 0.7 | 1.4 | 1.9 | 3.9 |
|  | 1500 | 0.3 | 0.6 | 0.5 | 1.0 | 0.5 | 1.0 | 1.1 | 2.2 | 1.2 | 2.4 | 2.4 | 4.9 |
|  | 1800 | . 5 | 1.0 | . 7 | 1.4 | . 8 | 1.6 | 1.5 | 3.1 | 1.7 | 3.5 | 2.8 | 5.7 |
|  | 2100 | . 7 | 1.4 | . 9 | 1.8 | 1.0 | 2.0 | 2.0 | 4.1 | 2.3 | 4.7 | 3.3 | 6.8 |
|  | $2400$ | . 8 | 1.6 | 1.1 | 2.3 | 1.3 | 2.7 | 2.5 | 5.1 | 2.8 | 5.7 | 3.7 | 7.6 |
|  | 3000 | 1.3 | 2.7 | 1.8 | 3.6 | 1.9 | 3.9 | 3.7 | 7.6 | 4.2 | 8.6 | 4.7 | 9.6 |
| 12" | 500 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- | 0.1 | 0.2 | 0.4 | 0.8 |
|  | 600 | ---- | ---- | ---- | ---- | ---- | -- | ---- | ---- | 0.2 | 0.4 | 0.5 | 1.0 |
|  | 700 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | --- | 0.2 | 0.4 | 0.6 | 1.2 |
|  | 800 | ---- | ---- | ---- | ---- | ---- | ---- | 0.1 | 0.2 | 0.2 | 0.4 | 0.6 | 1.2 |
|  | 900 | ---- | ---- | ---- | ---- | ---- | ---- | 0.2 | 0.4 | 0.2 | 0.4 | 0.7 | 1.4 |
|  | 1000 | ---- | ---- | ---- | ---- | 0.1 | 0.2 | 0.2 | 0.4 | 0.3 | 0.6 | 0.8 | 1.6 |
|  | 1200 | 0.1 | 0.2 | 0.1 | 0.2 | 0.2 | 0.4 | 0.3 | 0.6 | 0.3 | 0.6 | 1.0 | 2.0 |
|  | 1500 | 0.1 | 0.2 | 0.2 | 0.4 | 0.2 | 0.4 | 0.5 | 1.0 | 0.5 | 1.0 | 1.2 | 2.4 |
|  | 1800 | . 2 | . 4 | . 3 | . 6 | . 4 | . 8 | . 6 | 1.2 | . 7 | 1.5 | 1.5 | 3.1 |
|  | 2100 | . 3 | . 6 | . 4 | . 8 | . 4 | . 8 | . 8 | 1.6 | 1.0 | 2.0 | 1.7 | 3.5 |
|  | 2400 | . 4 | . 8 | . 5 | 1.0 | . 5 | 1.0 | 1.1 | 2.3 | 1.2 | 2.5 | 1.9 | 3.9 |
|  | 3000 | . 5 | 1.0 | . 7 | 1.5 | . 8 | 1.6 | 1.6 | 3.3 | 1.9 | 3.9 | 2.4 | 4.9 |
| 14" | 1000 | . 036 | . 074 | . 057 | . 116 | . 070 | . 143 | . 135 | . 276 | . 17 | . 35 | . 53 | 1.07 |
|  | 1500 | . 083 | . 170 | . 125 | . 256 | . 147 | . 301 | . 31 | . 64 | . 31 | . 63 | . 79 | 1.61 |
|  | 2000 | . 133 | . 27 | . 22 | . 45 | . 250 | . 51 | . 49 | 1.00 | . 55 | 1.13 | 1.05 | 2.15 |
|  | 2500 | . 200 | . 41 | . 32 | . 66 | . 37 | . 76 | . 70 | 1.43 | . 87 | 1.78 | 1.31 | 2.68 |
|  | 3000 | . 290 | . 59 | . 45 | . 92 | . 51 | 1.04 | 1.04 | 2.13 | 1.26 | 2.58 | 1.57 | 3.21 |
|  | 4000 | . 50 | 1.02 | . 79 | 1.62 | . 93 | 1.90 | 1.60 | 3.27 | 2.03 | 4.15 | 2.30 | 4.70 |
| 16" | 1000 | . 018 | . 037 | . 03 | . 06 | . 035 | . 072 | . 068 | . 139 | . 106 | . 217 | . 32 | . 65 |
|  | 2000 | . 069 | . 141 | . 11 | . 23 | . 126 | . 258 | . 25 | . 51 | . 27 | . 55 | . 63 | 1.29 |
|  | 3000 | . 151 | . 31 | . 23 | . 47 | . 26 | . 53 | . 52 | 1.06 | . 63 | 1.29 | . 991 | 2.02 |
|  | 4000 | . 26 | . 53 | . 40 | . 82 | . 44 | . 90 | . 85 | 1.74 | 1.04 | 2.13 | . 26 | 2.58 |
|  | 5000 | . 40 | . 82 | . 61 | 1.25 | . 66 | 1.35 | 1.26 | 2.58 | 1.53 | 3.13 | 1.70 | 3.48 |

## RESISTANCE OF VALVES AND FITTING TO FLOW OF NON-VISCOUS LIQUIDS

(At very high liquid viscosities and relatively low flow rates, resistances may be less than shown.)


## COMPUTING SUCTION and DISCHARGE CONDITIONS

## SECOND PROCEDURE (Using the Hydraulic Institute friction loss curves)

The following form may be used for analyzing the Intake and Discharge head conditions in conjunction with the Hydraulic Institute friction loss curves on the following pages. The viscosity and the specific gravity of the liquid at lowest pumping temperature must be known to use these curves. For viscosity and specific gravity values of common liquids, refer to Pages 23 and 24.

## ANALYZING THE INTAKE SYSTEM

1. Maximum Vertical Suction Lift $\qquad$
2. Suction Pipe Size Total Length $=$ $\qquad$ Ft. (See Page 11 For Equivalent Length of Fittings.)
3. Number of Elbows $\qquad$ @ $\qquad$ Ft. $=$ $\qquad$ Ft.
4. Number of Valves @ $\qquad$ Ft. = $\qquad$ Ft.
5. Strainer __ @ _ Ft. = $\qquad$ Ft.
6. Other Fittings __ @ $\qquad$ Ft. = $\qquad$ Ft.
7. $\qquad$ Ft. = $\qquad$ Ft.
8. Total Equivalent Length of Pipe: $\qquad$ Ft. (Add values 2 thru 7 )
9. Friction Modulus (From pages 13 thru 19 ) = $\qquad$
10. Friction Loss $=2.31 \times($ $\qquad$ ) $\times($ $\qquad$ $) \div 100$ $\qquad$ Ft. of Liquid
11. Total Suction Lift = (value $10+$ value 1 ) $\qquad$ Ft. of Liquid
NOTE: When 1 is a lift, add 1 to 10 . When 1 is a positive head, subtract 1 from 10.
12. Total Suction Lift in Ft. of Water $=\left(\frac{}{\text { Sp. Gr. }}\right) \times\left(\frac{}{\text { value } 11}\right)$ $\qquad$ Ft. of Water
13. Vacuum in inches of $\mathrm{Hg}=\left(\frac{}{\text { value } 12}\right) \div 1.13$ $\qquad$ In. Hg

NOTE: To determine if the pump will perform satisfactorily at this vacuum, refer to the Blackmer Vapor Pressure Graphs 50/1.

## ANALYZING THE DISCHARGE SYSTEM

14. Vertical Discharge Head $\qquad$ Ft. of Liquid
15. Discharge Pipe Size To
(See Page 11 For Equivalent Length of Fittings.)
16. Number of Elbows $\qquad$ Ft. $=$ $\qquad$ Ft.
17. Number of Valves $\qquad$ $\mathrm{Ft} .=$ $\qquad$ Ft.
18. Other Fittings _ @ _ _

Ft. $=$ $\qquad$ Ft.
19.
$\qquad$ @ $\qquad$ Ft. = $\qquad$ Ft .
20 $\qquad$ Ft. =
$\qquad$ Ft.
21. Total Equivalent Length of Pipe
=
$\qquad$
$\qquad$ Ft. (Add values 15 thru 20)
22. Friction Modulus (From Pages 13 thru 19)=
23. Friction Loss $=2.31 \times\left(\frac{}{\text { value } 21}\right) \times\left(\frac{}{\text { value } 22}\right) \div 100$
$\qquad$ Ft. of Liquid
24. Total Discharge Head $=\left(\frac{}{\text { value } 14}\right)+\left(\frac{}{\text { value } 23}\right)$ $\qquad$ Ft. of Liquid
25. Total Discharge Head in Ft. of Water $=\left(\frac{}{\text { Sp. Gr. }}\right) \times\left(\frac{}{\text { value } 24}\right)$ $\qquad$ Ft. of Water
26. Discharge Pressure in PSI $=(\underset{\text { Ft. of Water }}{ }) \div 2.31$ $\qquad$ PSI
27. Total Dynamic Head $\left(\frac{}{\text { value } 25}\right)+\left(\frac{}{\text { value } 12}\right)=$ $\qquad$ Ft. of Water
28. Differential Pressure $=\left(\frac{}{\text { value } 27}\right) \div 2.31$ $\qquad$
$\qquad$ PSI
29. Horsepower Required - (Refer to Blackmer Characteristic Curves printed separately) $\qquad$ HP

## PIPE FRICTION CURVES

IMPORTANT: Friction values shown in the following charts are for new, clean steel or wrought iron pipes having schedule 40 wall thickness. No allowance has been made for abnormal conditions of interior surface nor for deterioration from age. Roughness of interior surfaces of pipe does not affect the friction loss in laminar flow unless the open area has been reduced. In turbulent flow, however, friction loss is very much affected by roughness. It is recommended that when using 15-year-old pipe of average roughness, friction loss values in the turbulent area as shown on the charts be multiplied by 1.4.

HOW TO USE THESE CURVES: First find the chart that pertains to the correct pipe size. Then move upward along the vertical GPM line corresponding to the proper delivery rate until it intersects the diagonal line indicating the viscosity of the liquid to be pumped. Move horizontally from this point to the left hand scale and read the modulus value for this condition. For example, pumping a 1000 SSU liquid at 10 GPM through 1 -inch pipe would have a modulus of 48 . The actual friction loss per 100 feet of pipe may then be determined in PSI or in feet of liquid according to the formulae below. Notice there are many conditions where the diagonal viscosity lines reach the "limit" lines before intersecting all of the vertical GPM lines (such as 100 SSU at 20 GPM on the 1 -inch chart). In these cases it is necessary to continue upward along the proper limit line until it intersects the vertical. Thus in the example of 100 SSU at 20 GPM, the modulus would be 20 .


## PIPE FRICTION CURVES - 11⁄2" and $11 / 2^{" ~ S T E E L ~ P I P E ~}$

IMPORTANT: Friction values shown in the following charts are for new, clean steel or wrought iron pipes having schedule 40 wall thickness. No allowance has been made for abnormal conditions of interior surface nor for deterioration from age. Roughness of interior surfaces of pipe does not affect the friction loss in laminar flow unless
the open area has been reduced. In turbulent flow, however, friction loss is very much affected by roughness. It is recommended that when using 15 -year-old pipe of average roughness, friction loss values in the turbulent area as shown on the charts be multiplied by 1.4. (For information on how to use these curves, see page 13.)
FRICTION LOSS MODULUS FOR 100 FEET OF PIPE
Loss in lbs. per sq. in. = Modulus $X$ Specific Gravity



IMPORTANT: Friction values shown in the following charts are for new, clean steel or wrought iron pipes having schedule 40 wall thickness. No allowance has been made for abnormal conditions of interior surface nor for deterioration from age. Roughness of interior surfaces of pipe does not affect the friction loss in laminar flow unless
the open area has been reduced. In turbulent flow, however, friction loss is very much affected by roughness. It is recommended that when using 15-year-old pipe of average roughness, friction loss values in the turbulent area as shown on the charts be multiplied by 1.4. (For information on how to use these curves, see page 13.)


## PIPE FRICTION CURVES - 3" and 4" STEEL PIPE

IMPORTANT: Friction values shown in the following charts are for new, clean steel or wrought iron pipes having schedule 40 wall thickness. No allowance has been made for abnormal conditions of interior surface nor for deterioration from age. Roughness of interior surfaces of pipe does not affect the friction loss in laminar flow unless
the open area has been reduced. In turbulent flow, however, friction loss is very much affected by roughness. It is recommended that when using 15 -year-old pipe of average roughness, friction loss values in the turbulent area as shown on the charts be multiplied by 1.4. (For information on how to use these curves, see page 13.)
FRICTION LOSS MODULUS FOR 100 FEET OF PIPE
Loss in lbs. per sq. in. = Modulus $\times$ Specific Gravity


## PIPE FRICTION CURVES - 6" and 8" STEEL PIPE

IMPORTANT: Friction values shown in the following charts are for new, clean steel or wrought iron pipes having schedule 40 wall thickness. No allowance has been made for abnormal conditions of interior surface nor for
deterioration from age. Roughness of interior surfaces of pipe does not affect the friction loss in laminar flow unless
the open area has been reduced. In turbulent flow, however, friction loss is very much affected by roughness. It is recommended that when using 15-year-old pipe of average roughness, friction loss values in the turbulent area as shown on the charts be multiplied by 1.4. (For information on how to use these curves, see page 13.)



## PIPE FRICTION CURVES - 10" and 12" STEEL PIPE

IMPORTANT: Friction values shown in the following charts are for new, clean steel or wrought iron pipes having schedule 40 wall thickness. No allowance has been made for abnormal conditions of interior surface nor for deterioration from age. Roughness of interior surfaces of pipe does not affect the friction loss in laminar flow unless
the open area has been reduced. In turbulent flow, however, friction loss is very much affected by roughness. It is recommended that when using 15-year-old pipe of average roughness, friction loss values in the turbulent area as shown on the charts be multiplied by 1.4. (For information on how to use these curves, see page 13.)
FRICTION LOSS MODULUS FOR 100 FEET OF PIPE
Loss in lbs. per sq. in. = Modulus $X$ Specific Gravity



## PIPE FRICTION CURVES - 14" and 16" STEEL PIPE

IMPORTANT: Friction values shown in the following charts are for new, clean steel or wrought iron pipes having schedule 40 wall thickness. No allowance has been made for abnormal conditions of interior surface nor for deterioration from age. Roughness of interior surfaces of pipe does not affect the friction loss in laminar flow unless
the open area has been reduced. In turbulent flow, however, friction loss is very much affected by roughness. It is recommended that when using 15-year-old pipe of average roughness, friction loss values in the turbulent area as shown on the charts be multiplied by 1.4. (For information on how to use these curves, see page 13.)


## SELECTING PUMP CONSTRUCTION

1. SOLUTION TO BE PUMPED (Give common name, where possible, such as aviation gasoline, No. 2 fuel oil, perchlorethylene, etc.)
2. PRINCIPAL CORROSIVES $\left(\mathrm{H}_{2} \mathrm{SO}_{4}, \mathrm{HCL}\right.$, etc.)
(In the case of mixtures, state definite percentages by weight. For example: mixture contains $2 \%$ acid, in terms of 96.5\% $\mathrm{H}_{2} \mathrm{SO}_{4}$.)\% by weight
3. pH (if aqueous solution) ..... at ..... F
4. IMPURITIES OR OTHER CONSTITUENTS NOT GIVEN IN "2" (List amounts of any metallic salts, such as chlorides, sulphates, sulphides, chromates, and any organic materials which may be present, even though in percentages as low as $.01 \%$. Indicate, where practical, whether they act as accelerators or inhibitors on the pump material.)
5. SPECIFIC GRAVITY (solution pumped) ..... at ..... F
6. TEMPERATURE OF SOLUTION: maximum F, minimum F, normal ..... F
7. VAPOR PRESSURES AT ABOVE TEMPERATURES: maximum.............. minimum ............ normal (Indicate units used, such as pounds gauge, inches water, millimeters mercury.)
8. VISCOSITY SSU; or centistokes; at ..... F
9. AERATION: air-free partial saturated

$\qquad$
Does liquid have tendency to foam?

$\qquad$10. OTHER GASES IN SOLUTIONppm, orcc per liter11. SOLIDS IN SUSPENSION: (state types).......................................................................................................................
Specific gravity of solids
\% by weight
Quantity of solids
\% by weight
Particle size meshmesh ........................................................................................ \% by weightmesh\% by weightCharacter of solids: pulpy........................ gritty .......................... hard .................... soft ...................................
12. CONTINUOUS OR INTERMITTENT SERVICE
Will pump be used for circulation in closed system or for transfer?Will pump be operated at times against closed discharge?If intermittent, how often is pump started?Will pump be flushed and drained when not in service?
13. TYPE OF MATERIAL IN PIPE LINES TO BE CONNECTED TO PUMP
14. IS METAL CONTAMINATION UNDESIRABLE?
15. PREVIOUS EXPERIENCE Have you pumped this solution previously?
If so, of what material or materials was pump made?Service life in months?In case of trouble, what parts were affected?
Was trouble primarily due to corrosion? ..... erosion?
galvanic action?
Was attack uniform? $\qquad$ If localized, what parts were involved?
If galvanic action, name materials involved
If pitted, describe size, shape and location (A sketch will be helpful in an analysis of problem.)

## 16. WHAT IS CONSIDERED AN ECONOMIC LIFE?

(If replacement does not become too frequent, the use of inexpensive pump materials may be the most economical.)

MISCELLANEOUS CONVERSION FACTORS
To convert from
Atmospheres Atmospheres Barrels (U.S. liq.) Barrels
B.T.U.
Centimeters
Centimeters
Centimeters/sec
Centimeters/sec
Centipoises
Centistokes
Cubic centimeters
Cubic centimeters
Cubic centimeters
Cubic feet
Cubic feet/min
Cubic inches
Cubic inches
Cubic inches
Cubic meters
Cubic meters
Cubic meters
Cubic meters
Cubic meters $/ \mathrm{hr}$
Degrees
Dynes
Dynes/sq. cm.
Fathom
Feet
Feet of water
Feet of water Feet of water
Feet/hr
Feet/min
Feet/min
Feet/second
Foot pounds
Foot pounds/min
Gallons
Gallons
Gallons
Gallons
Horsepower Horsepower Inches
Inches
Inches
Inches
Inches of Hg
Inches of Hg
Inches of Hg
Kilograms
Kilograms/sq. cm Kilograms/sq. mm
Liters
Meters
Meters
Poise
Pounds water
psi
psi
Square inches
Square inches
Square inches
Square millimeters
Tons molasses/hr

To
Feet of water
Inches of Mercury

$$
\begin{aligned}
& \text { Gallons (U.S.) } \\
& \text { Gallons (U.S.) }
\end{aligned}
$$

H.P. hr.
feet
inches
feet/min.
feet/sec.
stokes
cu. ft.
cu. in. gallons (liq.)
cubic in.
g.p.m.
gallons.
cubic cm
cubic ft .
gallons (liq.)
cu. cm.
cu. ft.
cu. in.
Revolutions.
Pounds
psi
feet
meters
atmosphere
psi
inches of H
meters/min.
miles/hour
miles per hour
H.P. hr.

Horsepower
cubic cm.
cubic in.
gallon (Imp.)
cu. ft.
cu. ft./min.
ft . lbs./min.
ft . lbs
feet
feet
meters
millimeters
mils
atmospheres
ft . of water
psi
pounds (avdp.)
psi
gallons
gallons
feet
inches
centipoise
gallons atmospheres Inches of Hg.
feet of water
sq. cm .
sq. ft.
sq. mm.
sq. in.
g.p.m.

Multiply by

### 14.7 33.9

33.9
29.9
31.5
42.0
.0003929
.03280 .39370
1.96840
.03280
.01
.01
$3.5314 \times 10^{-5}$
.061020
.0002642
7.4805
1728.
7.4805
.004329
16.3870
.0005787
264.17
$1 \times 10^{6}$
35.31
$61,023.74$
4.403 .00277778
.00277778
$2.24809 \times 10^{-6}$ $1.45038 \times 10^{-5}$
6.
30.48006 . 3048006 .02949 .43300 . 88265 . 00018939 . 30480 .01136 .681818
$3.0303 \times 10^{-5}$
3,785.43
231.
$\qquad$ .13368 .13368
33,000
550. .083333 .0254 25.40005 1000. .033327
1.1309 .4890
2.2046
14.2233
1422.330 .264178
3.2808
39.3700
100.00
.11985
.06804
2.31000
6.4516
.006944
645.1630
.0015499
2.78

## COMPARATIVE LIQUID EQUIVALENTS

| Measures | Measure and Weight Equivalents of Items in First Column |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| and <br> Weights <br> for Comp. U.S | Imperial | Cubic | Cubic | Cubic | Liter | Pound <br> Gallon | Inch |
| Foot | Meter |  | Water |  |  |  |  |
| U.S. Gal. | 1. | .833 | 231. | .1337 | .00378 | 3.785 | 8.33 |
| Imp. Gal. | 1.20 | 1. | 277.42 | .1604 | .00454 | 4.546 | 10. |
| Cubic In. | .0043 | .00360 | 1. | .00057 | .000016 | .0163 | .0358 |
| Cubic Ft. | 7.48 | 6.229 | 1728. | 1. | .02827 | 28.312 | 62.355 |
| Cubic M. | 264.17 | 220.00 | 61023. | 35.319 | 1. | 1000. | 2200.54 |
| Liter | .26417 | .2200 | 61.023 | .0353 | .001 | 1. | 2.2005 |
| Pound $\mathrm{H}_{2} \mathrm{O}$ | .12 | .1 | 27.72 | .016 | .00045 | .454 | 1. |

## PRESSURE EQUIVALENTS

1 atmosphere =
760 millimeters of mercury at $32^{\circ} \mathrm{F}$.
14.7 pounds per square inch.
29.921 inches of mercury at $32^{\circ} \mathrm{F}$.

2116 pounds per square foot.
1.033 kilograms per square centimeter.
33.947 feet of water at $62^{\circ} \mathrm{F}$.

1 foot of air at $32^{\circ} \mathrm{F}$. and barometer $29.92=$
.0761 pound per square foot.
.0146 inch of water at $62^{\circ} \mathrm{F}$.
1 foot of water at $62^{\circ} \mathrm{F}=$
.433 pound per square inch.
62.355 pounds per square foot.
.883 inch of mercury at $62^{\circ} \mathrm{F}$.
821.2 feet of air at $62^{\circ} \mathrm{F}$. and barometer 29.92.

1 inch of water $62^{\circ} \mathrm{F}=$
.0361 pound per square inch.
5.196 pounds per square foot.
.5776 ounce per square inch.
.0735 inch of mercury at $62^{\circ} \mathrm{F}$.
68.44 feet of air at $62^{\circ} \mathrm{F}$. and barometer 29.92.

1 pound per square inch =
2.0355 inches of mercury at $32^{\circ} \mathrm{F}$.
2.0416 inches of mercury at $62^{\circ} \mathrm{F}$.
2.309 feet of water at $62^{\circ} \mathrm{F}$.
.07031 kilogram per square centimeter.
.06804 atmosphere.
51.7 millimeters of mercury at $32^{\circ} \mathrm{F}$.

HORSEPOWER - TORQUE CONVERSION
Horsepower $=\underline{\text { Torque (in lb. ft.) }} \underset{525 \mathrm{RPM}}{ }$
5250
FAHRENHEIT - CENTIGRADE CONVERSION TABLE

| Fahr. | Centi. | Fahr, | Centi. | Fahr. | Centi. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| -20 | -28.9 | 88 | 31.1 | 196 | 91.1 |
| -18 | -27.8 | 90 | 32.2 | 198 | 92.2 |
| -16 | -26.7 | 92 | 33.3 | 200 | 93.3 |
| -14 | -25.6 | 94 | 34.4 | 202 | 94.4 |
| -12 | -24.4 | 96 | 35.6 | 204 | 95.6 |
| -10 | -23.3 | 98 | 36.7 | 206 | 96.7 |
| -8 | -22.2 | 100 | 37.8 | 208 | 97.8 |
| -6 | -21.1 | 102 | 38.9 | 210 | 98.9 |
| -4 | -20. | 104 | 40. | 212 | 100. |
| -2 | -18.9 | 106 | 41.1 | 214 | 101.1 |
| 0 | -17.8 | 108 | 42.2 | 216 | 102.2 |
| 2 | -16.7 | 110 | 43.3 | 218 | 103.3 |
| 4 | -15.6 | 112 | 44.4 | 220 | 104.4 |
| 6 | -14.4 | 114 | 45.6 | 222 | 105.6 |
| 8 | -13.3 | 116 | 46.7 | 224 | 106.7 |
| 10 | -12.2 | 118 | 47.8 | 226 | 107.8 |
| 12 | -11.1 | 120 | 48.9 | 228 | 108.9 |
| 14 | -10. | 122 | 50. | 230 | 110. |
| 16 | -8.9 | 124 | 51.1 | 232 | 111.1 |
| 18 | -7.8 | 126 | 52.2 | 234 | 112.2 |
| 20 | -6.7 | 128 | 53.3 | 236 | 113.3 |
| 22 | -5.6 | 130 | 54.4 | 238 | 114.4 |
| 24 | -4.4 | 132 | 55.6 | 240 | 115.6 |
| 26 | -3.3 | 134 | 56.7 | 242 | 116.7 |
| 28 | -2.2 | 136 | 57.8 | 244 | 117.8 |
| 30 | -1.1 | 138 | 58.9 | 246 | 118.9 |
| 32 | 0. | 140 | 60. | 248 | 120. |
| 34 | 1.1 | 142 | 61.1 | 250 | 121.1 |
| 36 | 2.2 | 144 | 62.2 | 252 | 122.2 |
| 38 | 3.3 | 146 | 63.3 | 254 | 123.3 |
| 40 | 4.4 | 148 | 64.4 | 256 | 124.4 |
| 42 | 5.6 | 150 | 65.6 | 258 | 125.6 |
| 44 | 6.7 | 152 | 66.7 | 260 | 126.7 |
| 46 | 7.8 | 154 | 67.8 | 262 | 127.8 |
| 48 | 8.9 | 156 | 68.9 | 264 | 128.9 |
| 50 | 10. | 158 | 70. | 266 | 130. |
| 52 | 11.1 | 160 | 71.1 | 268 | 131.1 |
| 54 | 12.2 | 162 | 72.2 | 270 | 132.2 |
| 56 | 13.3 | 164 | 73.3 | 272 | 133.3 |
| 58 | 14.4 | 166 | 74.4 | 274 | 134.4 |
| 60 | 15.6 | 168 | 75.6 | 276 | 135.6 |
| 62 | 16.7 | 170 | 76.7 | 278 | 136.7 |
| 64 | 17.8 | 172 | 77.8 | 280 | 137.8 |
| 66 | 18.9 | 174 | 78.9 | 282 | 138.9 |
| 68 | 20. | 176 | 80. | 284 | 140. |
| 70 | 21.1 | 178 | 81.1 | 286 | 141.1 |
| 72 | 22.2 | 180 | 82.2 | 288 | 142.2 |
| 74 | 23.3 | 182 | 83.3 | 290 | 143.3 |
| 76 | 24.4 | 184 | 84.4 | 292 | 144.4 |
| 78 | 25.6 | 186 | 85.6 | 294 | 145.6 |
| 80 | 26.7 | 188 | 86.7 | 296 | 146.7 |
| 82 | 27.8 | 190 | 87.8 | 298 | 147.8 |
| 84 | 28.9 | 192 | 88.9 | 300 | 148.9 |
| 86 | 30. | 194 | 90. |  |  |

## VISCOSITY DEFINITIONS

The pump selection and application outline on page 3 calls attention to the importance of determining the type and viscosity of liquids to be handled. The following definitions should prove helpful in studying these characteristics.

Viscosity is that property of a liquid which resists any force tending to produce motion between its adjacent particles. Viscosity is usually measured by an instrument called a Viscosimeter. The Saybolt Viscosimeter is commonly used in the United States. A Saybolt Universal machine is used for liquids of medium viscosity, and a Saybolt Furol is used for those of higher viscosity. These viscosity ratings are expressed in Seconds Saybolt Universal (SSU) or Seconds Saybolt Furol (SSF). The viscosity, as determined by this type of Viscosimeter, is known as kinematic viscosity. This is not a true measure of a liquid's viscosity but is affected by the specific gravity of the liquid. The effect of specific gravity on viscosity determination can best be illustrated by visualizing two viscosity cups side by side, each containing a liquid of different specific gravity but of the same true viscosity. When a hole is opened in the bottom of each cup, liquid will run through because of the pull of gravity on the liquid. The one with the highest specific gravity will be pulled through the orifice at a higher rate; therefore, its viscosity will be expressed in less seconds than the lighter liquid whereas their true viscosity is the same. The force required to overcome viscosity of a liquid flowing through a pipe is not dependent on the specific gravity of a liquid but on its true or absolute viscosity. For this reason in computing pipe friction it is necessary to multiply the SSU viscosity by the specific gravity in order to arrive at the friction loss.

Blackmer sales engineers use a form of computing pressure and vacuum at the pump. This form contains a space for the insertion of the static head or lift which is expressed in feet of liquid. The friction tables which are based on SSU also give values expressed in feet of liquid. After these two values are added together to get a total discharge head in feet of liquid, the sum is multiplied by the specific gravity which automatically corrects this value to true viscosity.

The viscosity of a liquid should not be confused with its specific gravity. The specific gravity of a liquid is its weight compared to the weight of an equal volume of pure water both measured at a temperature of $60^{\circ}$ Fahrenheit. The viscosity of all liquids varies appreciably with changes in temperature, usually decreasing when the liquid is heated. This makes the knowledge of the pumping temperature of the liquid a very important factor. Consideration must also be given to the fact that a heated liquid may have a
relatively low viscosity when the pump is in operation. However, when the pump is shut down, the liquid which then remains in the pump will be subject to cooling, and its viscosity will increase accordingly. In many cases it will become so thick and sticky that the pump cannot be turned, in which case it is necessary to apply heat by means of steam connected to jacketed head pumps that "thaw out" the liquid which has "set up" in the pump prior to operation.
The effect of agitation on viscous liquids varies according to the type of liquid. The most common types are:

1. Newtonian liquids - such as water and mineral oils which are referred to as "true liquids", and their viscosity or consistency is not affected by agitation at a constant temperature.
2. Thixotropic liquids - are those which reduce their viscosity as the agitation is increased at a constant temperature. Examples of this type of liquid are asphalts, cellulose, glue, paints, greases, soap, starches, tars, printing ink, resin, varnish, vegetable oil, shortening, lacquer, wax, lard, etc.
3. Dilatant liquids - are those whose viscosity increases as the agitation is increased at a constant temperature. Examples are clay, slurry, candy compounds, and some starches. Most dilatant liquids will return to their original viscosity as soon as agitation ceases. Some liquids may change from thixotropic to dilatant or vice versa as the temperature of concentration is varied.
4. Colloidal liquids - are those which act like thixotropic liquids but will not recover their original viscosity when agitation is stopped. Colloidal solutions of soaps in water or oils at low viscosities, lotions, shampoos, and gelatinous compounds are in this class.
5. Rheopectic liquids - are those whose apparent viscosity increase with time to some maximum value at any constant rate of agitation.
The viscosity of the liquid is a very important factor in the selection of the proper pump for the installation. It is the determining factor in pipe friction and the power and speed requirements of the unit. Frequently when pumping liquids with high viscosity, it is necessary to use a larger pump operating at a slower speed.

VISCOSITY \& SPECIFIC GRAVITY OF COMMON LIQUIDS

| LIQUID | *SPECIFIC GRAVITY AT $60^{\circ} \mathrm{F}$. | VISCOSITIES IN SSU AT VARIOUS TEMPERATURES |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $30^{\circ} \mathrm{F}$ | $60^{\circ} \mathrm{F}$ | $80^{\circ} \mathrm{F}$ | $100^{\circ} \mathrm{F}$ | $130^{\circ} \mathrm{F}$ | $170^{\circ} \mathrm{F}$ | $210^{\circ} \mathrm{F}$ | $250^{\circ} \mathrm{F}$ |
| Corn Starch Solutions |  |  |  |  |  |  |  |  |  |
| 22 Baumé | 1.18 | 190 | 160 | 144 | 130 | 115 | 99 | 88 | 79 |
| 24 Baumé | 1.20 | 1,025 | 680 | 550 | 440 | 330 | 240 | 178 | 140 |
| 25 Baumé | 1.21 | 3,600 | 1,745 | 1,170 | 800 | 500 | 295 | 187 | 130 |
| Freon | $\begin{array}{r} 1.37 \text { to } 1.49 \\ \% 70^{\circ} \mathrm{F} \\ \hline \end{array}$ |  |  |  |  |  |  |  |  |
| Glycerin 99\% Soluble |  | 10,200 | 2,260 | 1,190 | 620 | 280 | 128 | 74 | 54 |
| Glycerin 100\% | 1.26\% 68${ }^{\circ} \mathrm{F}$ | 21,000 | 4,200 | 1,700 | 813 | 325 | 130 | 74 | 52 |
| Glycol: |  |  |  |  |  |  |  |  |  |
| Propylene | 1.038 @ 68${ }^{\circ} \mathrm{F}$ |  |  | $240 @ 70^{\circ}$ |  |  |  |  |  |
| Triethylene | 1.125 @ 68${ }^{\circ} \mathrm{F}$ |  |  | 185 @ $70^{\circ}$ |  |  |  |  |  |
| Diethylene | 1.12 |  |  | 149 @ $70^{\circ}$ |  |  |  |  |  |
| Ethylene | 1.125 |  |  | 88 @ $70^{\circ}$ |  |  |  |  |  |
| $\begin{gathered} \text { Glucose - Corn Products } \\ 2 \text { Star } \end{gathered}$ | 1.35 to 1.44 |  |  |  |  | 12,500 | 1,500 | 340 | 121 |
| Glucose - Corn Products <br> 3 Star | 1.35 to 1.44 |  |  |  |  | 10,200 | 2,400 | 750 | 300 |
| Honey - (Raw) |  |  |  |  | 340 |  |  |  |  |
| Hydrochloric Acid | 1.05 @ 68${ }^{\circ} \mathrm{F}$ |  |  |  |  |  |  |  |  |
| Ink - Newspaper |  | 65,000 | 20,000 | 10,000 | 5,500 | 2,400 | 1,025 | 500 | 280 |
| Ink - Printers | 1.00 to 1.38 |  | 100,000 | 30,300 | 12,500 | 3,800 | 1,100 | 420 | 200 |
| Kerosene | 78 to 82 |  |  |  | 32.6 |  |  |  |  |
| Lard | . 96 |  |  |  | 287 | 160 | 91 | 62.5 | 49.5 |
| Mercury | 13.6 |  |  |  |  |  |  |  |  |
| Molasses |  |  |  |  |  |  |  |  |  |
| A. Max. | 1.40 to 1.46 | 42,500 | 22,500 | 15,000 | 10,000 | 5,900 |  |  |  |
| A. Min. |  | 9,000 | 3,600 | 2,100 | 1,300 | 700 |  |  |  |
| B. Max. | 1.43 to 1.48 |  |  |  | 60,000 | 15,000 |  |  |  |
| B. Min. |  | 70,000 | 22,000 | 10,900 | 6,500 | 3,000 |  |  |  |
| C. Max. | 1.46 to 1.49 |  |  |  | 250,000 | 75,000 |  |  |  |
| C. Min. |  |  | 90,000 | 35,000 | 17,000 | 6,000 |  |  |  |
| Oils - Auto. Lubricating |  |  |  |  |  |  |  |  |  |
| S.A.E. 10 Max. | . 880 to .935 | 4,400 | 1,090 | 430 | 240 | 120 | 66 |  |  |
| 20 Max. | . 880 to .935 | 6,900 | 1,650 | 750 | 400 | 185 | 90 | 57 |  |
| 30 Max . | . 880 to . 935 | 13,000 | 2,700 | 1,200 | 580 | 255 | 120 | 66 | 49 |
| 40 | . 880 to . 935 | 25,000 | 4,850 | 2,000 | 950 | 380 | 150 | 80 | 55 |
| 50 | . 880 to .935 | 58,000 | 10,000 | 3,700 | 1,600 | 600 | 220 | 105 | 67 |
| 60 | . 880 to .935 | 100,000 | 15,000 | 5,300 | 2,300 | 800 | 285 | 128 | 76 |
| 70 | . 880 to . 935 |  | 22,000 | 7,500 | 3,100 | 1,050 | 342 | 150 | 86 |
| 10 W | . 880 to .935 |  |  |  |  |  |  |  |  |
| 20 W | . 880 to .935 |  |  |  |  |  |  |  |  |
| Oil-Castor | . $96 \bigcirc 68^{\circ} \mathrm{F}$ | 35,000 | 7,500 | 3,200 | 1,500 | 600 | 228 | 116 | 73 |
| Oil - Chinawood | . 943 | 6,900 | 2,000 | 1,040 | 580 | 285 | 135 | 82 | 58 |
| Oil-Cocoanut | . 925 | 2,250 | 550 | 270 | 150 | 81 | 50.5 |  |  |
| Oil - Cod | . 928 | 2,350 | 620 | 310 | 175 | 92 | 55 |  |  |
| Oil - Corn | . 924 | 2,150 | 740 | 410 | 250 | 135 | 77.5 | 54.8 |  |
| Oil - Cotton | . 88 to . 925 | 1,590 | 525 | 295 | 176 | 100 | 61.5 |  |  |
| Oil - Cylinder - 600 W | . 82 to . 95 | 80,000 | 14,500 | 6,000 | 2,650 | 1,000 | 360 | 165 | 94 |
| Oil - Diesel Fuel No. 2D | . 82 to . 95 | 138 | 70 | 53.6 | 45.5 | 39 |  |  |  |
| Oil - Diesel Fuel No. 3D | . 82 to . 95 | 390 | 145 | 92 | 65 | 48 | 39 |  |  |
| Oil - Diesel Fuel No. 4D | . 82 to . 95 | 4,400 | 700 | 280 | 140 | 70 | 44.2 |  |  |
| Oil - Diesel Fuel No. 5D | . 82 to . 95 | 16,500 | 3,500 | 1,500 | 750 | 320 | 136 | 76.5 | 54 |
| Oil - Fuel No. 1 | . 82 to . 95 |  |  |  | 35 |  |  |  |  |
| Oil - Fuel No. 2 | . 82 to . 95 | 104 | 56 | 45.5 | 40 |  |  |  |  |
| Oil - Fuel No. 3 | . 82 to . 95 | 126 | 68 | 53 | 45 | 39 |  |  |  |
| Oil - Fuel No. 5A | . 82 to . 95 | 1,480 | 420 | 215 | 125 | 72 | 48 |  |  |
| Oil - Fuel No. 5B | . 82 to .95 | 850 | 600 | 490 | 400 | 315 | 235 | 178 | 141 |
| Oil - Fuel No. 6 | . 82 to . 95 |  | 72,000 | 21,500 | 7,800 | 2,150 | 590 | 225 | 110 |
| Oil - Fuel - Navy Spec. | . 989 Max. | 3,300 | 1,100 | 600 | 360 | 190 | 100 | 66 | 50.2 |
| Oil - Fuel - Navy II | 1.0 Max. |  | 24,000 | 8,600 | 3,500 | 1,150 | 370 | 160 | 89 |

[^0]VISCOSITY \& SPECIFIC GRAVITY OF COMMON LIQUIDS, cont.

| LIQUID | *SPECIFIC GRAVITY AT $60^{\circ} \mathrm{F}$. | VISCOSITIES IN SSU AT VARIOUS TEMPERATURES |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $30^{\circ} \mathrm{F}$ | $60^{\circ} \mathrm{F}$ | $80^{\circ} \mathrm{F}$ | $10{ }^{\circ} \mathrm{F}$ | $130^{\circ} \mathrm{F}$ | $170^{\circ} \mathrm{F}$ | $210^{\circ} \mathrm{F}$ | $250^{\circ} \mathrm{F}$ |
| Oil - Gas | . 887 | 205 | 89 | 62.5 | 50 | 41 |  |  |  |
| Oil - Insulating |  | 439 | 152 | 92 | 65 | 47.5 | 38.6 |  |  |
| Oil - Lard | . 912 to . 925 | 1,400 | 560 | 340 | 220 | 128 | 76 | 55.2 |  |
| Oil - Menhadden | 933 | 750 | 330 | 210 | 140 | 90 | 60.5 |  |  |
| Oil - Neats Foot | . 917 |  | 1.020 | 440 | 235 | 120 | 74 |  |  |
| Oil - Olive | . 912 to .918 | 1,500 | 550 | 320 | 200 | 115 | 70 | 51.5 |  |
| Oil - Palm | . 924 | 1,790 | 640 | 360 | 221 | 125 | 74 | 53 |  |
| Oil - Peanut | 920 | 1,325 | 515 | 300 | 195 | 112 | 69.5 | 51.5 |  |
| Oil-Quenching | None Given |  | 850 | 350 | 240 | 148 | 87 | 61 |  |
| Oil - Rape Seed | . 919 | 1,550 | 625 | 340 | 250 | 145 | 87 | 61.5 | 49.5 |
| Oil - Rosin | 980 | 35,400 | 7,600 | 3,200 | 1,500 | 600 | 238 | 115 | 72.5 |
| Oil - Rosin (Wood) | 1.09 Avg. |  |  |  |  |  |  | 9,000 | 750 |
| Oil - Sesame | . 923 | 1,150 | 470 | 282 | 184 | 110 | 69 | 52 | 44 |
| Oil - Soya Bean | . 927 to .98 | 1,320 | 470 | 265 | 165 | 96 | 60 |  |  |
| Oil-Sperm | . 883 | 400 | 215 | 150 | 110 | 78 | 57 |  |  |
| Oil - Turbine Heavy | . 91 Avg. | 4,800 | 1,280 | 625 | 350 | 170 | 86 | 57 |  |
| Oil - Turbine Light | . 91 Avg. | 770 | 330 | 208 | 138 | 87 | 58.8 |  |  |
| Oil - Whale | . 925 | 1.070 | 460 | 280 | 184 | 112 | 72 | 53.5 | 45 |
| Petrolatum | . 825 | 350 | 220 | 167 | 130 | 97 | 72 | 58 | 50 |
| Phenol (Carbolic Acid) | . 95 to 1.08 | 6 | 65@65 |  |  |  |  |  |  |
| Silicate of Soda, Baumé $41^{\circ}$ <br> Ratio $1: 3.3$ |  | 3,500 | 350 | 125 | 66 | 42.5 |  |  |  |
| $\begin{gathered} \hline \text { Silicate of Soda, Baumé } 41^{\circ} \\ \text { Ratio } 1: 3.22 \end{gathered}$ |  | 800 | 195 | 100 | 64 | 45 |  |  |  |
| Silicate of Soda, Baumé $42^{\circ}$ Ratio |  | 1,650 | 380 | 180 | 104 | 60.5 | 45.5 |  |  |
| Syrup - Corn - Karo |  |  | 60,000 | 15,500 | 5,000 | 1,300 | 350 | 136 |  |
| Syrup - Orange | None Given | 50,000 | 9,400 | 3,700 | 1,690 | 650 | 242 | 117 | 72.6 |
| Syrup - Corn $41^{\circ}$ Baumé | 1.395 |  | 70,000 | 25,000 | 11,000 | 3,600 | 1,100 | 450 | 225 |
| Syrup - Corn $42^{\circ}$ Baumé | 1.409 |  |  | 54,000 | 20,000 | 6,000 | 1,650 | 600 | 280 |
| Syrup - Corn $43^{\circ}$ Baumé | 1.423 |  |  |  | 42,500 | 10,000 | 2,200 | 700 | 300 |
| Syrup - Corn $44^{\circ}$ Baumé | 1.437 |  |  |  |  | 22,500 | 3,900 | 1,050 | 380 |
| Syrup - Corn $45^{\circ}$ Baumé | 1.450 |  |  |  |  | 55,000 | 7,000 | 1,460 | 480 |
| Syrups - Sugar: |  |  |  |  |  |  |  |  |  |
| 60 Brix. | 1.29 | 1,650 | 350 | 162 | 92 | 54.7 | 40.3 |  |  |
| 62 Brix. | 1.30 | 2,600 | 480 | 215 | 111 | 62 | 42.5 |  |  |
| 64 Brix. | 1.31 | 4,400 | 720 | 298 | 148 | 72 | 45.5 |  |  |
| 66 Brix. | 1.326 | 7,400 | 1,100 | 420 | 195 | 86 | 49.5 |  |  |
| 68 Brix. | 1.338 | 12,000 | 1,650 | 620 | 275 | 114 | 57.5 | 42.1 |  |
| 70 Brix. | 1.35 | 28,000 | 3,100 | 1,000 | 400 | 145 | 63.5 | 44 |  |
| 72 Brix. | 1.36 | 45,000 | 4,800 | 1,550 | 640 | 220 | 85 | 51.5 |  |
| 73 Brix. | 1.37 | 26,500 | 3,800 | 1,325 | 580 | 220 | 89 | 54 | 42.9 |
| 74 Brix. | 1.376 |  | 11,000 | 3,050 | 1,100 | 340 | 112 | 60 | 44.5 |
| 76 Brix. | 1.39 |  | 19,000 | 5,500 | 2,000 | 620 | 190 | 87.9 | 56 |
| Sweetose | None Given | 70,000 | 7,700 | 2,400 | 950 | 320 | 114 | 62 | 46 |
| Sulphuric Acid | 1.83 |  |  |  |  |  |  |  |  |
| Tallow | . 918 Avg. |  |  |  |  |  |  |  |  |
| Tar - Coke Oven | 1.12 + |  | 19,000 | 4,500 | 1,400 | 380 | 114 | 58.5 | 43.5 |
| *Tar - Gas House | 1.16 to 1.30 |  | 33,000 | 7,000 | 2,000 | 480 | 128 | 61 | 44 |
| Tar - Pine | 1.06 |  | 55,000 | 10,000 | 2,500 | 550 | 135 | 61.8 | 43.7 |
| Tar-Road-RT 2 | 1.07 | 14,000 | 2,800 | 1,180 | 580 | 250 | 107 | 63.6 | 49 |
| Tar-Road-RT 4 | 1.08 |  | 13,900 | 4,300 | 1,650 | 540 | 180 | 85 | 55 |
| Tar-Road-RT 6 | 1.09 |  | 80,000 | 19,500 | 5,900 | 1,400 | 350 | 130 | 71 |
| Tar-Road - RT 8 | 1.13 |  |  |  | 30,000 | 5,000 | 850 | 240 | 100 |
| Tar-Road-RT 10 | 1.14 + |  |  | FIGS. TOO HIGH FOR LOG PAPER |  |  |  |  |  |
| Tar-Road-RT 12 | 1.15 + |  |  | FIGS. TOO HIGH FOR LOG PAPER |  |  |  |  |  |
| Varnish - Spar | . 9 | 3,800 | 1,600 | 1,000 | 650 | 370 | 200 | 125 | 87 |

[^1]CONVERSION TABLE BAUMÉ-SPECIFIC GRAVITY-weight per gallon for liquids HEAVIER than water

| $\begin{gathered} \hline \text { A.P.I. } \\ \text { or } \\ \text { BAUMÉ } \end{gathered}$ | SPECIFIC GRAVITY | $\begin{array}{\|l\|} \hline \text { WGHT } \\ \text { PERR } \\ \text { GAL. } \end{array}$ | $\begin{array}{\|c\|} \hline \text { A.P.I. } \\ \text { or } \\ \text { BAUMÉ } \end{array}$ | SPECIFIC GRAVITY | $\begin{gathered} \text { WGHT. } \\ \text { PERR } \\ \text { GAL. } \end{gathered}$ | $\begin{gathered} \text { A.P.I. } \\ \text { or } \\ \text { BAUMÉ } \end{gathered}$ | SPECIFIC GRAVITY | $\begin{gathered} \text { WGHT. } \\ \text { PERR } \\ \text { GAL. } \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { A.P.I. } \\ \text { or } \\ \text { BAUMÉ } \end{array}$ | SPECIFIC GRAVITY | WGHT. PER GAL | $\begin{gathered} \text { A.P.I. } \\ \text { or } \\ \text { BAUMÉ } \end{gathered}$ | SPECIFIC GRAVITY | $\begin{gathered} \text { WGHT. } \\ \text { PER } \\ \text { GAL. } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 1.000 | 8.33 | 10 | 1.074 | 8.95 | 20 | 1.160 | 9.67 | 30 | 1.260 | 10.50 | 40 | 1.381 | 11.51 |
| 1 | 1.006 | 8.38 | 11 | 1.082 | 9.02 | 21 | 1.169 | 9.74 | 31 | 1.271 | 10.59 | 45 | 1.450 | 12.08 |
| 2 | 1.014 | 8.45 | 12 | 1.090 | 9.08 | 22 | 1.178 | 9.82 | 32 | 1.283 | 10.69 | 50 | 1.526 | 12.72 |
| 3 | 1.021 | 8.51 | 13 | 1.098 | 9.15 | 23 | 1.188 | 9.90 | 33 | 1.294 | 10.78 | 55 | 1.611 | 13.42 |
| 4 | 1.028 | 8.57 | 14 | 1.106 | 9.22 | 24 | 1.198 | 9.98 | 34 | 1.306 | 10.88 | 60 | 1.705 | 14.21 |
| 5 | 1.035 | 8.62 | 15 | 1.115 | 9.29 | 25 | 1.208 | 10.07 | 35 | 1.318 | 10.98 | 65 | 1.812 | 15.10 |
| 6 | 1.043 | 8.69 | 16 | 1.124 | 9.37 | 26 | 1.218 | 10.15 | 36 | 1.330 | 11.08 | 70 | 1.933 | 16.11 |
| 7 | 1.050 | 8.75 | 17 | 1.132 | 9.43 | 27 | 1.228 | 10.23 | 37 | 1.342 | 11.18 | ---- | ---- | ---- |
| 8 | 1.058 | 8.82 | 18 | 1.141 | 9.51 | 28 | 1.239 | 10.32 | 38 | 1.355 | 11.29 | ---- | ---- | ---- |
| 9 | 1.066 | 8.88 | 19 | 1.150 | 9.58 | 29 | 1.250 | 10.42 | 39 | 1.367 | 11.39 | ---- | ---- | ---- |

CONVERSION TABLE BAUMÉ-SPECIFIC GRAVITY-weight per gallon for liquids LIGHTER than water

| $\begin{gathered} \hline \text { A.P.I. } \\ \text { or } \\ \text { BAUMÉ } \end{gathered}$ | SPECIFIC GRAVITY | $\begin{array}{\|c\|} \hline \text { WGHT } \\ \text { PER } \\ \text { GAL. } \end{array}$ | $\begin{array}{\|c\|} \hline \text { A.P.I. } \\ \text { or } \\ \text { BAUMÉ } \end{array}$ | SPECIFIC GRAVITY | $\begin{gathered} \text { WGHT. } \\ \text { PERR } \\ \text { GAL. } \end{gathered}$ | $\begin{gathered} \text { A.P.I. } \\ \text { or } \\ \text { BAUMÉ } \end{gathered}$ | SPECIFIC GRAVITY | WGHT. PER GAL. | $\begin{array}{\|c\|} \hline \text { A.P.I. } \\ \text { or } \\ \text { BAUMÉ } \end{array}$ | SPECIFIC GRAVITY | WGHT PER GAL | $\begin{gathered} \text { A.P.I. } \\ \text { or } \\ \text { BAUMÉ } \end{gathered}$ | SPECIFIC GRAVITY | $\begin{gathered} \text { WGHT. } \\ \text { PERR } \\ \text { GAL. } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | 1.000 | 8.33 | 31 | 0.871 | 7.25 | 52 | 0.7712 | 6.42 | 73 | 0.6926 | 5.76 | 91 | . 636 | 5.29 |
| 11 | 0.993 | 8.27 | 32 | 0.865 | 7.21 | 53 | 0.7670 | 6.39 | 74 | 0.6893 | 5.73 | 92 | . 633 | 5.27 |
| 12 | 0.986 | 8.21 | 33 | 0.860 | 7.16 | 54 | 0.7637 | 6.35 | 75 | 0.6859 | 5.70 | 93 | . 630 | 5.25 |
| 13 | 0.979 | 8.16 | 34 | 0.855 | 7.12 | 55 | 0.7597 | 6.32 | 76 | 0.6826 | 5.68 | 94 | . 628 | 5.22 |
| 14 | 0.973 | 8.10 | 35 | 0.850 | 7.08 | 56 | 0.7556 | 6.28 | 77 | 0.6793 | 5.65 | 95 | . 625 | 5.20 |
| 15 | 0.966 | 8.04 | 36 | 0.845 | 7.03 | 57 | 0.7516 | 6.25 | 78 | 0.6750 | 5.62 | 96 | . 622 | 5.18 |
| 16 | 0.959 | 7.99 | 37 | 0.840 | 6.99 | 58 | 0.7476 | 6.22 | 79 | 0.6728 | 5.60 | 97 | . 619 | 5.15 |
| 17 | 0.953 | 7.94 | 38 | 0.835 | 6.95 | 59 | 0.7437 | 6.18 | 80 | 0.6696 | 5.57 | 98 | . 617 | 5.13 |
| 18 | 0.946 | 7.88 | 39 | 0.830 | 6.91 | 60 | 0.7398 | 6.15 | 81 | 0.6665 | 5.54 | 99 | . 614 | 5.11 |
| 19 | 0.940 | 7.83 | 40 | 0.825 | 6.87 | 61 | 0.7359 | 6.12 | 82 | 0.6634 | 5.52 | 100 | . 611 | 5.09 |
| 20 | 0.934 | 7.78 | 41 | 0.820 | 6.83 | 62 | 0.7310 | 6.09 | 83 | 0.6603 | 5.49 | ---- | ---- | ---- |
| 21 | 0.928 | 7.73 | 42 | 0.816 | 6.79 | 63 | 0.7283 | 6.06 | 84 | 0.6572 | 5.47 | ---- | ---- | ---- |
| 22 | 0.921 | 7.68 | 43 | 0.811 | 7.75 | 64 | 0.7246 | 6.03 | 85 | 0.6541 | 5.44 | ---- | ---- | ---- |
| 23 | 0.916 | 7.63 | 44 | 0.806 | 6.71 | 65 | 0.7209 | 5.99 | 86 | 0.6511 | 5.42 | ---- | ---- | ---- |
| 24 | 0.910 | 7.58 | 45 | 0.802 | 6.68 | 66 | 0.7172 | 5.96 | 87 | 0.6481 | 5.39 | ---- | ---- | ---- |
| 25 | 0.904 | 7.53 | 46 | 0.797 | 6.64 | 67 | 0.7136 | 5.93 | 88 | 0.6452 | 5.37 | ---- | ---- | ---- |
| 26 | 0.898 | 7.48 | 47 | 0.793 | 6.60 | 68 | 0.7090 | 5.90 | 89 | 0.6422 | 5.34 | ---- | ---- | ---- |
| 27 | 0.893 | 7.43 | 48 | 0.788 | 6.56 | 69 | 0.7065 | 5.87 | 90 | 0.6393 | 5.32 | ---- | ---- | ---- |
| 28 | 0.887 | 7.39 | 49 | 0.784 | 6.53 | 70 | 0.7020 | 5.85 | ---- | ---- | ---- | ---- | ---- | ---- |
| 29 | 0.882 | 7.34 | 50 | 0.780 | 6.49 | 71 | 0.6995 | 5.82 | ---- | ---- | ---- | ---- | ---- | ---- |
| 30 | 0.876 | 7.30 | 51 | 0.775 | 6.46 | 72 | 0.6950 | 5.79 | ---- | ---- | ---- | ---- | ---- | ---- |

The specific gravity of a substance is its weight as compared with the weight of an equal bulk of pure water.
For making specific gravity determinations the temperature of the water is usually taken at $62^{\circ} \mathrm{F}$. when 1 cubic foot of water weighs 62.355 lbs . Water is at its greatest density at $39.2^{\circ} \mathrm{F}$. or $4^{\circ}$ Centigrade.

## CONVERSION TABLE BRIX TO SPECIFIC GRAVITY AND BAUMÉ

| Brix | Sp. Gr. | Bé | Brix | Sp. Gr. | Bé | Brix | Sp. Gr. | Bé | Brix | Sp. Gr. | Bé | Brix | Sp. Gr. | Bé |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 1.00 | 0 | 24 | 1.101 | 13.35 | 48 | 1.220 | 26.30 | 64 | 1.314 | 34.64 | 79 | 1.410 | 42.10 |
| 2 | 1.01 | 1.13 | 26 | 1.110 | 14.45 | 50 | 1.230 | 27.38 | 66 | 1.326 | 35.66 | 80 | 1.420 | 42.60 |
| 4 | 1.02 | 2.24 | 28 | 1.120 | 15.54 | 51 | 1.238 | 27.91 | 68 | 1.340 | 36.67 | 82 | 1.430 | 43.50 |
| 6 | 1.02 | 3.37 | 30 | 1.130 | 16.63 | 52 | 1.244 | 28.43 | 70 | 1.351 | 37.66 | 84 | 1.440 | 44.50 |
| 8 | 1.03 | 4.49 | 32 | 1.140 | 17.73 | 53 | 1.249 | 28.96 | 71 | 1.357 | 38.17 | 86 | 1.460 | 45.44 |
| 10 | 1.04 | 5.60 | 34 | 1.150 | 18.81 | 54 | 1.255 | 29.48 | 72 | 1.364 | 38.66 | 88 | 1.470 | 46.40 |
| 12 | 1.046 | 6.71 | 36 | 1.160 | 19.90 | 55 | 1.261 | 30.00 | 73 | 1.370 | 39.16 | 90 | 1.480 | 47.30 |
| 14 | 1.057 | 7.81 | 38 | 1.170 | 20.98 | 56 | 1.267 | 30.53 | 74 | 1.376 | 39.65 | 92 | 1.500 | 48.20 |
| 16 | 1.066 | 8.94 | 40 | 1.180 | 22.10 | 57 | 1.272 | 31.05 | 75 | 1.383 | 40.15 | 94 | 1.510 | 49.10 |
| 18 | 1.074 | 10.04 | 42 | 1.190 | 23.13 | 58 | 1.278 | 31.56 | 76 | 1.389 | 40.64 | 96 | 1.530 | 50 |
| 20 | 1.083 | 11.15 | 44 | 1.200 | 24.20 | 60 | 1.290 | 32.60 | 77 | 1.396 | 41.12 | 98 | 1.540 | 51 |
| 22 | 1.092 | 12.30 | 46 | 1.210 | 25.26 | 62 | 1.302 | 33.60 | 78 | 1.403 | 41.61 | 100 | 1.560 | 52 |

## APPROXIMATE VISCOSITY COMPARISONS

The following tables list several commonly used viscosity measurements and permit quick, easy conversion from one to another. Although the values are only approximate, they are sufficiently accurate for most pump calculations. The tables are especially useful because all values may be compared directly with each other. Take particular notice that the absolute viscosities (centipoises) on the right-hand page depend on the specific gravity of the liquid. Hence, in dealing with centipoises (or poises), it is necessary to know the specific gravity in order to select viscosity values from the appropriate column on the right. For specific gravities not listed in the table, the absolute viscosity (in centipoises) may be found by multiplying the kinematic viscosity (in centistokes) by the specific gravity of the liquid.

KINEMATIC VISCOSITY

| SSF <br> SAYBOLT SECONDS FUROL | REDWOOD <br> NO. 1 <br> STANDARD <br> SECONDS | REDWOOD <br> NO. 2 <br> ADMIRALTY <br> SECONDS | ENGLER <br> SECONDS | ENGLER SPECIFIC <br> DEGREES | CENTISTOKES $\begin{aligned} & \text { (100 Centistokes } \\ & =1 \text { Stoke) } \end{aligned}$ | SSU <br> SAYBOLT SECONDS UNIVERSAL | FORD \#3 SECONDS | FORD \#4 SECONDS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10,000 | 91,300 | 9,130 | 144,000 | 2,880 | 21,000 | 100,000 | 8,750 | 5,670 |
| 9,000 | 82,100 | 8,210 | 130,000 | 2,590 | 18,900 | 90,000 | 7,860 | 5.100 |
| 8,000 | 73,000 | 7,300 | 120,000 | 2,300 | 16,800 | 80,000 | 7,000 | 4,540 |
| 7,000 | 64,000 | 6,400 | 100,000 | 2,010 | 14,700 | 70,000 | 6,120 | 3,970 |
| 6,000 | 54,900 | 5,490 | 86,500 | 1,730 | 12,600 | 60,000 | 5,240 | 3,420 |
| 5,000 | 45,700 | 4,570 | 72,000 | 1,440 | 10,500 | 50,000 | 4,370 | 2,840 |
| 4,500 | 41,100 | 4,110 | 64,500 | 1,295 | 9,450 | 45,000 | 3,930 | 2,550 |
| 4,000 | 36,500 | 3,680 | 60,000 | 1,150 | 8,500 | 40,000 | 3,500 | 2,270 |
| 3,500 | 32,000 | 3,200 | 50,000 | 1,000 | 7,350 | 35,000 | 3,060 | 1,990 |
| 3,000 | 27,400 | 2,760 | 45,000 | 860 | 6,300 | 30,000 | 2,620 | 1,710 |
| 2,500 | 22,800 | 2,280 | 36,000 | 720 | 5,250 | 25,000 | 2,180 | 1,420 |
| 2,000 | 18,400 | 1,840 | 30,000 | 580 | 4,250 | 20,000 | 1,750 | 1,140 |
| 1,500 | 13,700 | 1,370 | 21,500 | 430 | 3,150 | 15,000 | 1,310 | 855 |
| 1,000 | 9,000 | 900 | 15,000 | 290 | 2,200 | 10,000 | 875 | 567 |
| 900 | 8,000 | 800 | 13,000 | 260 | 1,950 | 9,000 | 786 | 510 |
| 800 | 7,100 | 710 | 12,000 | 235 | 1,700 | 8,000 | 700 | 454 |
| 700 | 6,200 | 620 | 10,500 | 210 | 1,500 | 7,000 | 612 | 397 |
| 600 | 5,400 | 540 | 9,000 | 180 | 1,300 | 6,000 | 524 | 342 |
| 500 | 4,300 | 430 | 7,500 | 150 | 1,050 | 5,000 | 437 | 284 |
| 400 | 3,600 | 360 | 5,500 | 115 | 850 | 4,000 | 350 | 227 |
| 300 | 2,600 | 260 | 4,500 | 88 | 630 | 3,000 | 262 | 171 |
| 200 | 1,800 | 195 | 3,000 | 58 | 420 | 2,000 | 175 | 114 |
| 100 | 900 | 90 | 1,500 | 31 | 220 | 1,000 | 87.5 | 56.7 |
| 90 | 800 | 80 | 1,300 | 27 | 195 | 900 | 78.6 | 51.0 |
| 80 | 710 | 71 | 1,200 | 24 | 170 | 800 | 70.0 | 45.4 |
| 70 | 620 | 62 | 1,050 | 21 | 150 | 700 | 61.2 | 39.7 |
| 60 | 540 | 54 | 900 | 18 | 130 | 600 | 52.4 | 34.2 |
| 50 | 430 | 43 | 750 | 14 | 105 | 500 | 43.7 | 28.4 |
| 40 | 340 | 36 | 550 | 11 | 85 | 400 | 35.0 | 22.7 |
| 33 | 260 | 26 | 450 | 9 | 63 | 300 | 26.2 | 17.1 |
| 24 | 195 | 20 | 300 | 6 | 42 | 200 | 17.5 | 11.4 |
| 15 | 90 |  | 150 | 3 | 22 | 100 | 8.8 | 5.7 |
|  | 80 |  | 130 |  | 19 | 90 | 7.9 | 5.1 |
|  | 70 |  | 120 |  | 17 | 80 | 7.0 | 4.5 |
|  | 62 |  | 100 |  | 15 | 70 | 6.1 | 4.0 |
|  | 54 |  | 90 |  | 10 | 60 | 5.2 | 3.4 |
|  | 43 |  | 75 |  | 7 | 50 | 4.4 | 2.8 |
|  | 36 |  | 55 |  | 4 | 40 | 3.5 | 2.3 |

ABSOLUTE VISCOSITY (For specific gravities listed below)

| CENTIPOISES (100 CENTIPOISES EQUAL 1 POISE) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FOR SPECIFIC GRAVITY OF 0.8 | FOR SPECIFIC GRAVITY OF 0.9 | FOR <br> SPECIFIC <br> GRAVITY <br> OF 1.0 | FOR <br> SPECIFIC GRAVITY OF 1.1 | FOR SPECIFIC GRAVITY OF 1.2 | FOR SPECIFIC GRAVITY OF 1.3 | FOR SPECIFIC GRAVITY OF 1.4 |
| 16,800 | 18,900 | 21,000 | 23,100 | 25,200 | 27,300 | 29,400 |
| 15,100 | 17,000 | 18,900 | 20,800 | 22,680 | 24,560 | 26,440 |
| 13,440 | 15,100 | 16,800 | 18,500 | 20,180 | 21,820 | 23,500 |
| 11,750 | 13,230 | 14,700 | 16,180 | 17,640 | 19,100 | 20,590 |
| 10,080 | 11,340 | 12,600 | 13,860 | 15,120 | 16,480 | 17,630 |
| 8,400 | 9,450 | 10,500 | 11,550 | 12,600 | 13,650 | 14,700 |
| 7,560 | 8,500 | 9,450 | 10,400 | 11,350 | 12,300 | 13,240 |
| 6,800 | 7,650 | 8,500 | 9,350 | 10,200 | 11,050 | 11,900 |
| 5,880 | 6,620 | 7,350 | 8,090 | 8,830 | 9,560 | 10,300 |
| 5,040 | 5,670 | 6,300 | 6,940 | 7,560 | 8,200 | 8,830 |
| 4,200 | 4,720 | 5,250 | 5,780 | 6,300 | 6,830 | 7,350 |
| 3,400 | 3,820 | 4,250 | 4,680 | 5,100 | 5,530 | 5,950 |
| 2,520 | 2,840 | 3,150 | 3,460 | 3,780 | 4,090 | 4,410 |
| 1,760 | 1,980 | 2,200 | 2,420 | 2,640 | 2,860 | 3,080 |
| 1,560 | 1,750 | 1,950 | 2,150 | 2,340 | 2,530 | 2,730 |
| 1,360 | 1,530 | 1,700 | 1,870 | 2,040 | 2,210 | 2,380 |
| 1,200 | 1,350 | 1,500 | 1,650 | 1,800 | 1,950 | 2,100 |
| 1,040 | 1,170 | 1,300 | 1,430 | 1,560 | 1,690 | 1,820 |
| 840 | 945 | 1,050 | 1.150 | 1,260 | 1,370 | 1,470 |
| 680 | 765 | 850 | 935 | 1,020 | 1,100 | 1,190 |
| 505 | 567 | 630 | 694 | 756 | 820 | 883 |
| 336 | 378 | 420 | 462 | 504 | 546 | 588 |
| 176 | 198 | 220 | 242 | 264 | 286 | 308 |
| 156 | 175 | 195 | 214 | 234 | 253 | 273 |
| 136 | 153 | 170 | 187 | 204 | 221 | 238 |
| 120 | 135 | 150 | 165 | 180 | 195 | 210 |
| 104 | 117 | 130 | 143 | 156 | 169 | 182 |
| 84 | 94 | 105 | 109 | 126 | 136 | 147 |
| 68 | 77 | 85 | 94 | 102 | 111 | 119 |
| 50 | 57 | 63 | 69 | 76 | 82 | 88 |
| 34 | 38 | 42 | 46 | 50 | 55 | 59 |
| 18 | 20 | 22 | 24 | 26 | 29 | 31 |
| 15 | 17 | 19 | 21 | 23 | 25 | 27 |
| 14 | 15 | 17 | 19 | 20 | 22 | 24 |
| 12 | 14 | 15 | 17 | 18 | 20 | 21 |
| 8 | 9 | 10 | 11 | 12 | 13 | 14 |
| 6 | 6 | 7 | 8 | 8 | 9 | 10 |
| 3 | 4 | 4 | 4 | 5 | 5 | 6 |


[^0]:    * Depends on origin, or percent and type of solvent used.

[^1]:    * Depends on origin, or percent and type of solvent used.

